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**HYDROGEOLOGIC ASSESSMENT
AT CLEAR LAKES GRADE
FEDERAL-AID PROJECT RS-2709(006)
GOODING COUNTY, IDAHO**

Prepared for:

**Sharp and Smith Consulting Engineers and Surveyors
327 N. 27th Street
Boise, ID 83702**

Prepared by:

**Chen-Northern, Inc.
Boise, ID**

October 1991

2214 North 4th Avenue
PO Box 2601
Tri-Cities, Washington 99302
509 547-1011
509 547-1013 Facsimile

DRAFT

October 2, 1991

Sharp and Smith Engineers
327 N. 27th Street
Boise, ID 83702

Attention: Mr. John Sharp, P.E.

Subject: Report of Hydrogeologic Assessment at
Clear Lakes Grade, Gooding County, Idaho

Gentlemen:

Enclosed is our report summarizing the findings of our hydrogeologic assessment conducted at Clear Lakes Grade in Gooding County, Idaho.

If you have any questions regarding the contents of this report, please feel free to contact us at your convenience.

Respectfully submitted,

Steven A. Narkiewicz, P.E.
Division Manager

SAN/jw
Enclosure

**HYDROGEOLOGIC ASSESSMENT
AT CLEAR LAKES GRADE
GOODING COUNTY, IDAHO**

EXECUTIVE SUMMARY

A hydrogeologic assessment was conducted at Clear Lakes Grade in Gooding County, Idaho to characterize the hydrologic conditions in the vicinity and render an opinion on the potential changes in surface and groundwater conditions as a result of roadway construction. The proposed roadway will originate at the Snake River and proceed northeast approximately one-half mile where a fill section up to 140 feet thick and a cut section approximately 100 feet deep will be required to raise the southern section of the roadway through the canyon rim. North of the canyon the roadway continues north for a total length of about 2.2 miles. The proposed alignment intercepts numerous spring flows and streams below the canyon rim and several irrigation canals to the north.

Results of the investigation have been summarized below:

- ◆ The local stratigraphy consists of several sequences of basalt flows, separated by sand and gravel sedimentary interbeds.
- ◆ Groundwater is approximately 75 to 95 feet below ground surface (BGS) and will be intercepted by the road cut. A second water bearing unit, present at depths ranging from 185 to 200 feet BGS, will apparently not affect construction activities.
- ◆ Channels or conduits will be necessary to transmit as much as 107 CFS of water from irrigation canals S Coulee, S39 and S27 in the northern portion of the alignment.
- ◆ Drainage structures should be constructed to channel as much as 3 to 5 CFS of water beneath fill slopes on the south portion of the roadway. Additional drainage measures will be necessary to dewater the marsh located between stations 26+50 and 28+50.
- ◆ Up to 3.5 CFS of irrigation water will need to be diverted from the east side of the alignment between stations 51+00 and 60+00.
- ◆ Based on preliminary calculations and computer modelling, the road cut at the canyon rim will generate a steady-state flow of approximately 0.03 to 1 CFS; the first figure represents a flow rate based on measured hydraulic conductivity at the site and the second figure was calculated using an average hydraulic conductivity for fractured basalt obtained from the literature. Several factors may increase the discharge at the road cut from the measured value (0.03 CFS) including increased hydraulic conductivity at the road cut due to blasting, mass removal (load relaxation) resulting in widening of existing fractures at the road cut face, lateral increases in hydraulic conductivity from that measured, effects of drought over the last five years on "normal" water levels

versus those measured, and flushing of sediment from fractures at the road cut face. Accounting for these factors and using a safety factor of 10 times, a reasonable flow rate from the road cut for conveyance design may be 0.5 CFS.

- ◆ The road cut will depress the upper aquifer for a distance of approximately 2000 feet. The Madalena domestic and cellar water wells will lose about one foot of water due to road cut dewatering. Other area wells should not be affected. Blasting during construction may cause additional damage to uncased area wells.

- ◆ The springs at Clear Lakes Trout Hatchery, located about 6000 feet west of the road cut, should not be affected by construction activities.

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1.0 INTRODUCTION

This report presents the findings of the hydrogeologic assessment conducted at Clear Lakes Grade in Gooding County, Idaho. The report provides Sharp and Smith Consulting Engineers and Surveyors with information concerning the hydrogeologic conditions present in the vicinity of the proposed alignment of Secondary Highway Route 2709 (Clear Lakes Grade) at the time of this investigation.

1.1 Purpose and Scope

The purpose of the assessment is to characterize the present hydrologic conditions in the vicinity and render an opinion on the potential changes in surface and groundwater conditions as a result of roadway construction. The primary tasks of this investigation were to:

- o Drill seven exploratory borings and collect representative subsoil and rock samples to characterize the subsurface materials beneath the site;
- o Install groundwater monitoring wells in all seven borings to provide access to determine the groundwater migration direction and hydraulic properties of the water-bearing units underlying the site and for obtaining water-quality samples;
- o Submit representative water samples to an EPA approved laboratory for analysis to document basic groundwater constituents;
- o Install piping and weirs in ten locations to measure discharges from local springs and drainages;
- o Conduct aquifer performance tests in selected monitoring wells;
- o Conduct a well records and water rights search to identify potential groundwater usages within a one mile radius of the site; and

- o Prepare a report summarizing the results of the field investigation.

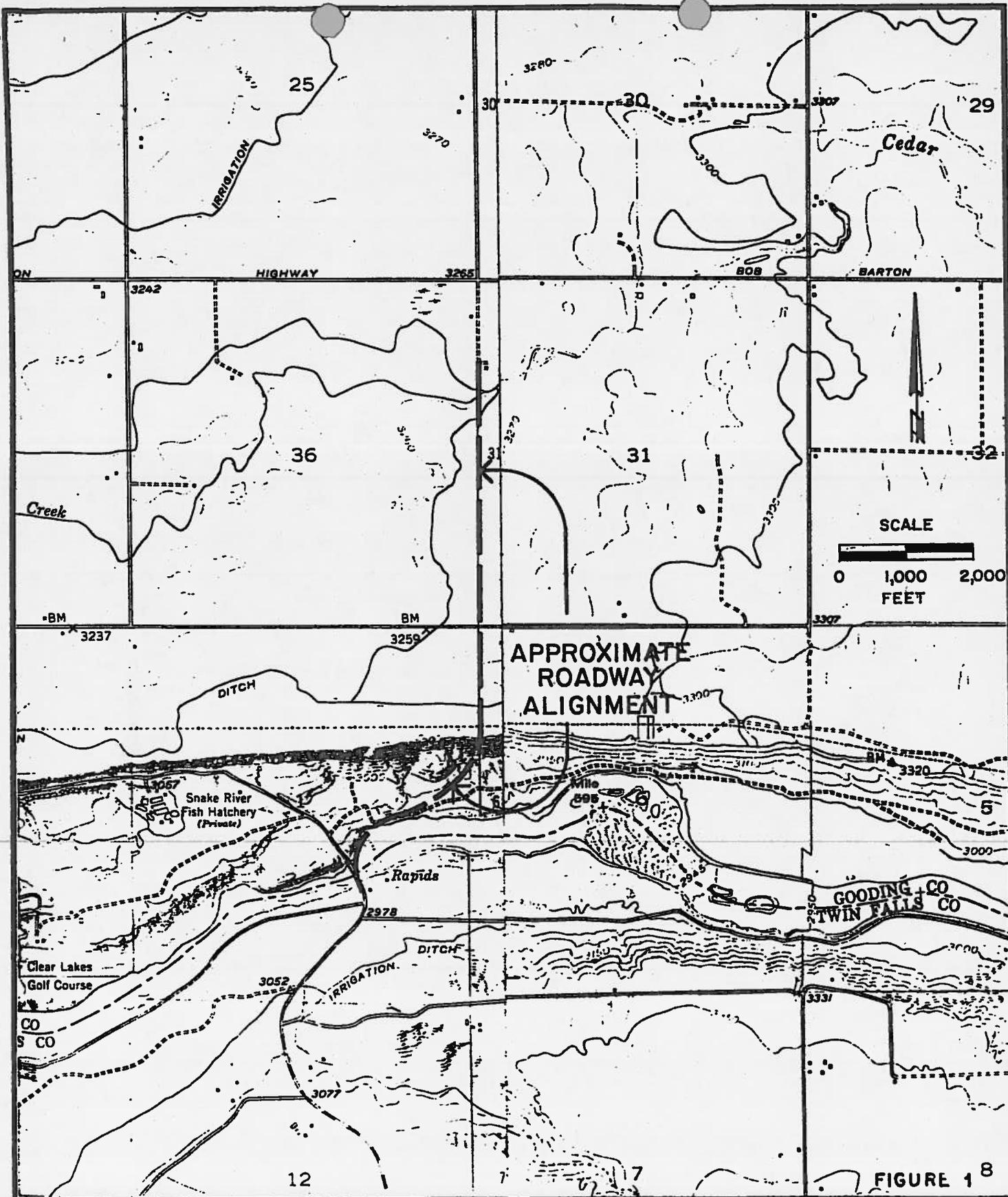
2.0 SITE DESCRIPTION

The proposed Secondary Highway Route 2709 (Clear Lakes Grade) is located north of the Snake River between Mileposts 10.5 and 12.5 of the existing secondary highway route 2709 in Gooding County, Idaho (See Figure 1). The proposed project consists of a two to three lane roadway with a maximum grade of about seven percent. The proposed roadway will originate at the Snake River and proceed northeast approximately one-half mile across gently sloping irrigated agricultural land. A fill section up to 140 feet thick and a cut section approximately 100 feet deep will be required to construct the southern section of the roadway through the canyon rim. North of the canyon the roadway continues north across relatively level farm land for a total length of about 2.2 miles.

The site is surrounded on the north, south, and east by irrigated farming and ranching properties. Clear Lakes Country Club and Golf Course is located approximately one-half mile west of the site along the Snake River. Clear Lakes Fish Hatchery is situated along the northwest portion of the golf course. The hatchery receives its water from springs which emerge along the base of the canyon rim approximately one mile west of the proposed roadway alignment.

2.1 Geology

Gooding County lies along the south-central portion of the Snake River Plain subdivision of the Columbia Plateau physiographic province. The Snake River Plain is characterized by successive



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**VICINITY MAP
CLEAR LAKES GRADE**

GOODING COUNTY

IDAHO

DATE
SEPT. 1991

DRAWN

JFZ

REVIEWED

PTS

SCALE

AS SHOWN

DRAWING NO.

190-1496

Quaternary basaltic lava flows of the Snake River Group, which are occasionally separated by alluvial, eolian, or volcanoclastic interbeds (IDHW, 1985).

The site lies within the transition zone between the eastern and western subdivision of the Snake River Plain (Street and DeTar, 1987). The oldest volcanic rocks exposed in the area are part of the Tertiary Banbury Basalt member of the Idaho Group (Malde and Powers, 1962). In the study area, the Banbury Basalt lies on a sequence of unconsolidated sand and gravel which exceeds 80 feet in thickness, and is overlain by a second sedimentary unit consisting of approximately 100 feet of slightly indurated sand and gravel of indeterminate age.

A series of younger, unaltered basalt flows and sedimentary interbeds of the Quaternary Snake River Group uncomfortably overlie Idaho Group formations. In the project area, the Thousand Springs Basalt Formation of the Snake River Group forms the prominent basalt cliffs and accompanying plateau which define the north side of the Snake River Canyon (Malde and Powers, 1962). This plateau is covered by a thin veneer of unconsolidated sediments.

The youngest lithologic unit in the area consists of cross-bedded coarse-grained cobbles and boulders identified by Malde and Powers (1962) as the Melon Gravel. The Melon Gravel was deposited in the Snake River Canyon during the Bonneville flood in late Pleistocene time. The Melon Gravel is locally covered by fine grained sand and silt of eolian and alluvial origin.

2.2 Hydrogeology

The study area is located near the western margin of the Snake River Plain Aquifer. The Snake River is the primary drainage in the area and has incised a steep walled canyon several hundred feet deep along the southern boundary of Gooding County. On the north

side of the canyon, numerous springs emerge from the canyon walls. Springs on the north bank of the Snake River Between Milner Dam, located approximately 20 miles east of Twin Falls and downstream to Hagerman include 11 of the 65 springs in the United States with discharges exceeding 100 CFS (Thomas, 1968).

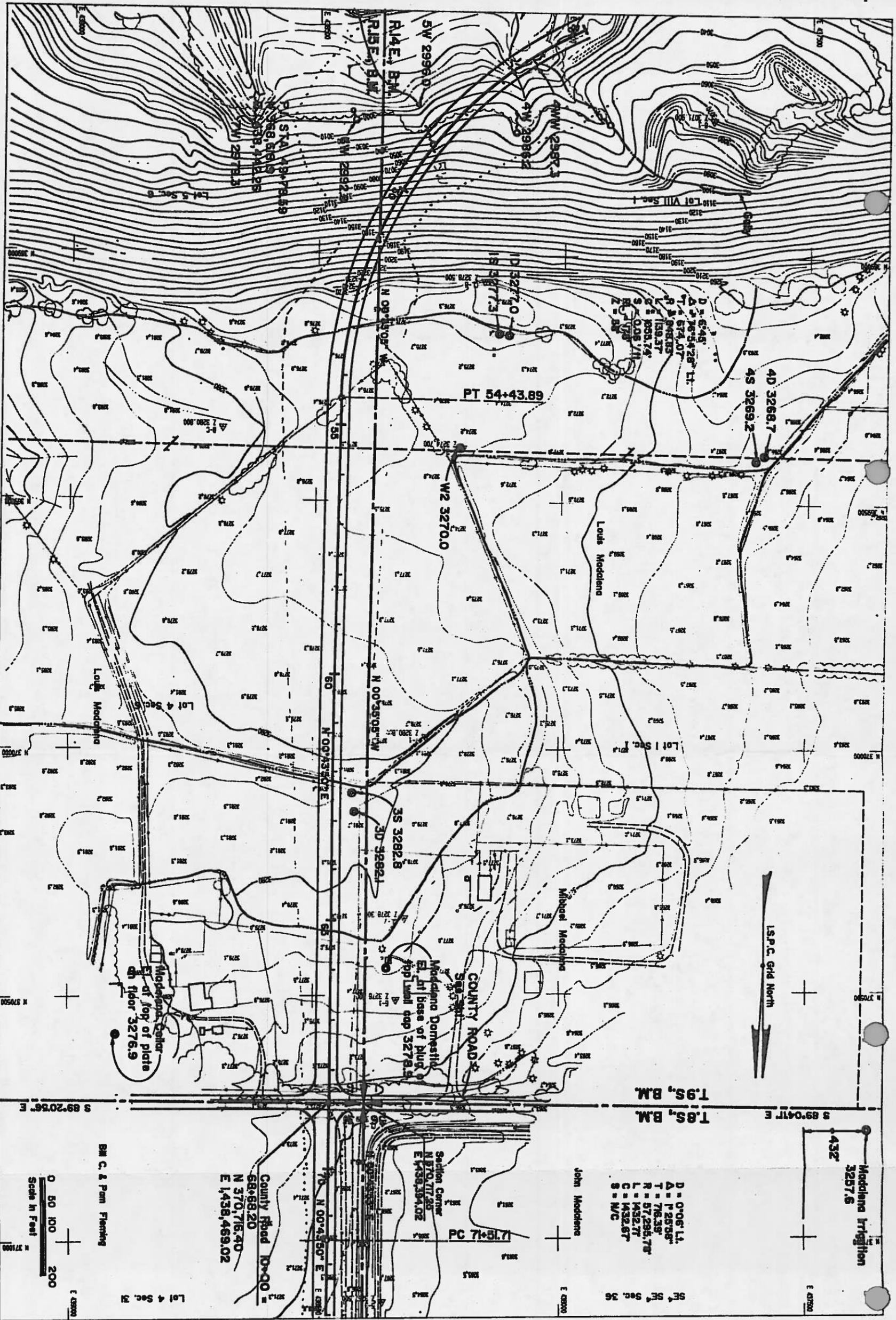
The regional aquifer is recharged by stream flow from the mountains to the north, seepage from upstream portions of the Snake River, precipitation, and infiltration from unlined irrigation canals (Thomas, 1968). A potentiometric surface map of the regional aquifer indicates that the local groundwater flows from east to west (IDHW, 1985).

3.0 FIELD INVESTIGATION

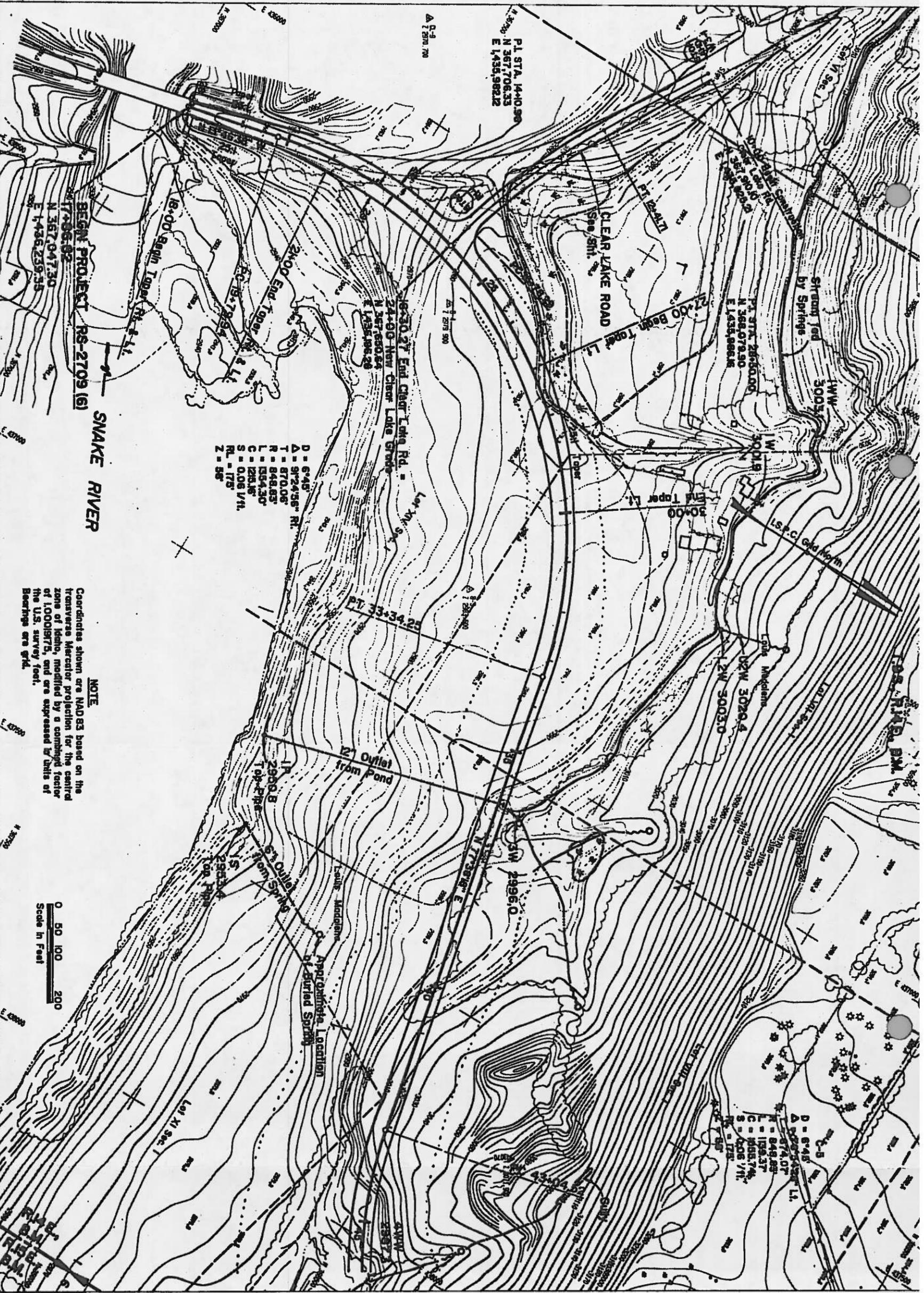
The field investigation consisted of drilling seven exploratory borings, completing all borings as monitoring wells, and collecting water samples for laboratory analysis. Aquifer performance tests were conducted on selected wells to estimate hydraulic conductivities. Piping and weirs were installed at several locations below the canyon rim to evaluate discharges from springs and drainages. Water quality samples were obtained from the springs in an attempt to correlate these discharges with samples different aquifers.

3.1 Drilling and Subsurface Sample Collection

On March 19 through April 4, 1991, a truck-mounted air rotary drill rig with an eight inch hammer bit was used for advancing seven exploratory borings in the area north of the basalt escarpment. All borings were completed as monitoring wells.



NO. DATE BY		REVISIONS		DESIGNED		SCALE SHOWN		IDaho		FEDERAL AID PROJECT NO.	
DESCRIPTION		DESIGN CHECKED		CADD FILE NO.		AREA FOR 34" X 22" PRINTS ONLY		TRANSPORTATION DEPARTMENT		REGION 10 IDAHO	
DETAILED		DRAWING DATE						IDaho		SHEET 2 OF 2	
DRAWING DATE								IDaho		FORM CATALOG NUMBER 26-0182100	
								IDaho		COUNTY	
								IDaho		KEY NUMBER	
								IDaho		FIGURE 2B	



D = 6'48"
 T = 870.06'
 R = 848.83'
 L = 1504.30'
 C = 1204.18'
 S = 0.06 V/H.
 RL = 175'
 Z = 95'

NOTE
 Coordinates shown are NAD83 based on the Transverse Mercator projection for the central zone of Idaho, modified by a combined factor of 1.00018775, and are expressed in units of the U.S. survey foot.
 Bearings are gnl.



- LEGEND**
- ~ Head of Spring
 - Elev. Top of Weir Plate
 - Elev. Top of PVC Well Liner
 - Elev. Top of PVC Weir
 - Perennial Stream
 - Intermittent Stream or Irrigation Channel
 - Marsh
 - ⊠ Test Boring



REVISIONS

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SCALES SHOWN ARE FOR 34" X 22" PRINTS ONLY

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DRAWING DATE:

FEDERAL AID PROJECT NO.

REGION 10 IDAHO

DATE: SEPT. 1981

Clear-Worthen, Inc.
 SITE MAP
 CLEAR LAKE GRADE
 Gooding County, Idaho
 COUNTY: 26-0182100
 SHEET 1 OF 2

FIGURE 2A

IDAHO TRANSPORTATION DEPARTMENT



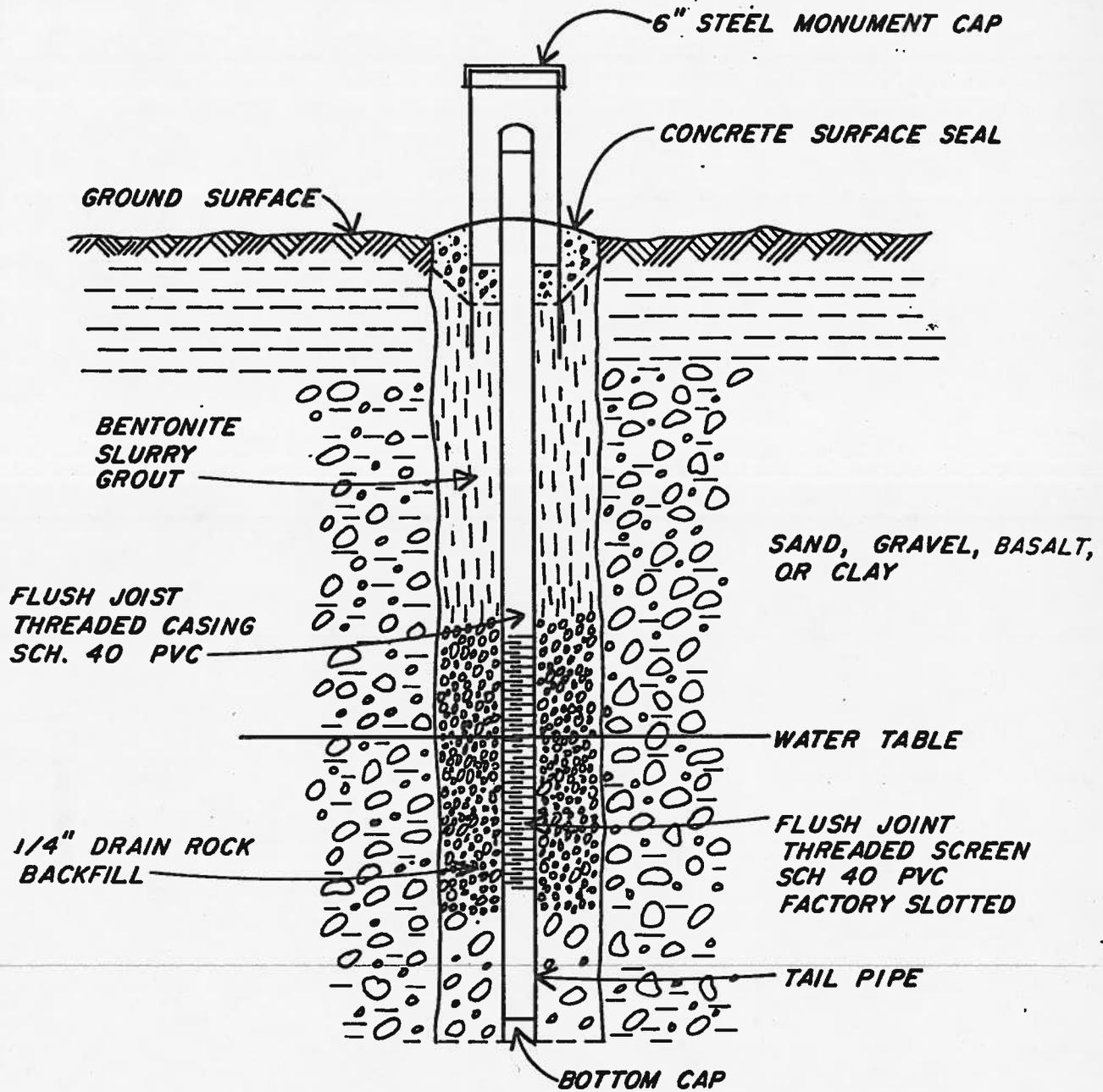
On August 19 through 22, 1991, an exploratory boring was advanced using rotary methods. Continuous core samples were obtained using a truck-mounted rotary drill rig. A one inch diameter PVC pipe was placed in the boring for temporary monitoring of groundwater levels. Figures 2A and 2B display the location of monitoring wells and other significant project features. Appendix A presents field observations, lithologic logs and sample collection methods.

3.2 Well Construction

Monitoring wells were installed in each boring using completion methods summarized in Appendix A. Figure 3 presents a schematic diagram of typical monitoring well construction.

During drilling, monitoring wells MW-1S, MW-3S, and MW-4S were installed where groundwater was initially encountered at approximately 80 to 100 feet BGS. Below this initial saturated zone, the moisture content of drill cuttings indicated that groundwater was also present at depths below about 180 to 200 feet BGS. Monitoring wells MW-1D, MW-3D, and MW-4D were completed in this interval. Well No. MW-2 was advanced to 400 feet and screened from 230 to 250 feet BGS.

On July 9, 1991, a survey was conducted by McCarter, Tuller and Chronic, Inc. (presently re-organized as Sharp and Smith) to determine the locations and elevations of the top of the well casings. Monitoring wells were developed using a mechanical bailer. Static water levels were measured periodically between April and September, 1991 to determine the groundwater migration direction and hydraulic gradient and evaluate changes in water levels throughout the irrigation season.



SCHEMATIC SHOWING TYPICAL MONITORING WELL CONSTRUCTION DETAIL

FIGURE 3

Chen-Northern, Inc.

DETAIL OF TYPICAL MONITORING WELL CONSTRUCTION

DATE	DRAWN	REVIEWED	SCALE	DRAWING NO.
SEPT. 1991	JFZ	PTS	NTS	190-1496

Table 1 presents a summary of well completion and groundwater elevation data from the monitoring well network and selected local domestic and irrigation wells. Figure 4 depicts water level fluctuations throughout the irrigation season in monitoring well numbers MW-1S, MW-3S, and MW-4S, completed within the shallow aquifer. Figure 5 presents similar information for wells within the deeper saturated zones (MW-1D, MW-2, MW-3D, and MW-4D).

3.3 Flow Measurements of Springs and Drainages

Visual reconnaissance of the study area identified at least 11 springs flowing from the slope below the basalt escarpment. Measuring stations were constructed in drainages below the springs during March and April, 1991. In four of the springs (2WU, 2WL, 5W, and 6W), water was diverted to a 4 inch PVC pipe for measurement. Six drainages were fitted with 90 degree V-notch weirs (1WW, 1W, 3W, 4W, 4WW, and 7W). At location 1W, a Stevens chart recorder was installed to provide a continuous record of water level fluctuations.

TABLE 1
Groundwater Monitoring Well Data
(elevation in feet)

<u>Well ID</u>	<u>Date</u>	<u>Depth to Water Level BTOC¹</u>	<u>Elevation of Static Water Level</u>	<u>Screened Interval BGS²</u>
MW-1S	3-28-91	88.83	3188.47	80'-100'
	4-12-91	89.22	3188.08	
	5-03-91	77.20	3200.10	
	5-24-91	73.32	3203.98	
	6-06-91	73.47	3203.83	
	6-19-91	76.63	3200.67	
	7-16-91	74.40	3202.90	
	8-01-91	72.65	3204.65	
	8-15-91	73.07	3204.23	
	9-10-91	73.35	3203.95	
9-18-91	74.66	3202.64		

TABLE 1 CONT.

<u>Well ID</u>	<u>Date</u>	<u>Depth to Water Level BTOC¹</u>	<u>Elevation of Static Water Level</u>	<u>Screened Interval BGS²</u>
MW-1D	3-28-91	196.92	3080.08	182'-207'
	4-12-91	197.07	3079.93	
	5-03-91	197.04	3079.96	
	5-24-91	196.35	3080.65	
	6-06-91	196.20	3080.80	
	7-16-91	196.10	3080.90	
	8-01-91	196.02	3080.98	
	8-15-91	195.98	3081.02	
	9-10-91	195.68	3081.32	
	9-18-91	195.75	3081.25	
MW-2	3-28-91	195.57	3074.43	230'-249'
	4-12-91	195.72	3074.28	
	5-03-91	195.74	3074.26	
	5-24-91	195.20	3074.80	
	6-06-91	194.98	3075.02	
	7-16-91	195.01	3074.99	
	8-01-91	194.82	3075.18	
	8-15-91	194.67	3075.33	
	9-11-91	194.04	3075.96	
	9-18-91	194.28	3075.72	
MW-3S	4-12-91	91.18	3191.62	89'-109'
	5-03-91	92.27	3190.53	
	5-11-91	92.57	3190.23	
	5-24-91	92.11	3190.69	
	6-06-91	91.97	3190.83	
	6-19-91	92.21	3190.59	
	7-16-91	91.70	3191.10	
	8-01-91	90.60	3192.20	
	8-15-91	89.83	3192.97	
9-11-91	87.57	3195.23		
	9-18-91	87.17	3195.63	
MW-3D	4-12-91	184.98	3097.12	193'-212'
	5-03-91	186.03	3096.07	
	5-11-91	185.66	3096.44	
	5-24-91	185.09	3097.01	
	6-06-91	184.78	3097.32	
	7-16-91	184.67	3097.43	
	8-01-91	184.03	3098.07	
	8-15-91	183.77	3098.33	
	9-11-91	182.94	3099.16	
	9-18-91	183.05	3099.05	

TABLE 1 CONT.

<u>Well ID</u>	<u>Date</u>	<u>Depth to Water Level BTOC¹</u>	<u>Elevation of Static Water Level</u>	<u>Screened Interval BGS²</u>
MW-4S	4-12-91	81.75	3187.45	85'-104'
	5-03-91	79.55	3189.65	
	5-24-91	74.78	3194.42	
	6-06-91	75.32	3193.88	
	6-19-91	76.40	3192.80	
	7-16-91	75.15	3194.05	
	8-01-91	74.59	3194.61	
	8-15-91	75.20	3194.00	
	9-11-91	73.75	3195.45	
	9-18-91	76.25	3192.95	
MW-4D	4-12-91	182.66	3086.04	182'-202'
	5-03-91	182.54	3086.16	
	5-24-91	182.09	3086.61	
	6-06-91	181.85	3086.85	
	7-16-91	182.04	3086.66	
	8-01-91	181.77	3086.93	
	8-15-91	181.73	3086.97	
	9-18-91	181.28	3087.42	
Madalena Domestic	3-28-91	88.16	3190.74	Open Hole Below 19'
	4-12-91	86.16	3192.74	
	5-03-91	88.18	3190.72	
	5-24-91	88.26	3190.64	
	6-06-91	88.25	3190.65	
Madalena Cellar	3-28-91	83.20	3193.70	Unknown
	4-12-91	83.20	3193.70	
	5-03-91	85.03	3191.87	
	5-24-91	85.04	3191.86	
	6-06-91	85.07	3191.83	
Madalena Irrigation	3-28-91	71.00	3186.60	Open Hole Below 19'
	4-12-91	71.00	3186.60	
	5-03-91	72.27	3185.33	
	5-28-91	72.42	3185.18	
	6-06-91	72.48	3185.12	

¹ - Below top of casing
² - Below ground surface

HYDROGRAPH OF SHALLOW MONITORING WELLS
 MW-1S, MW-3S, AND MW-4S
 1991 GROUNDWATER MONITORING PROGRAM

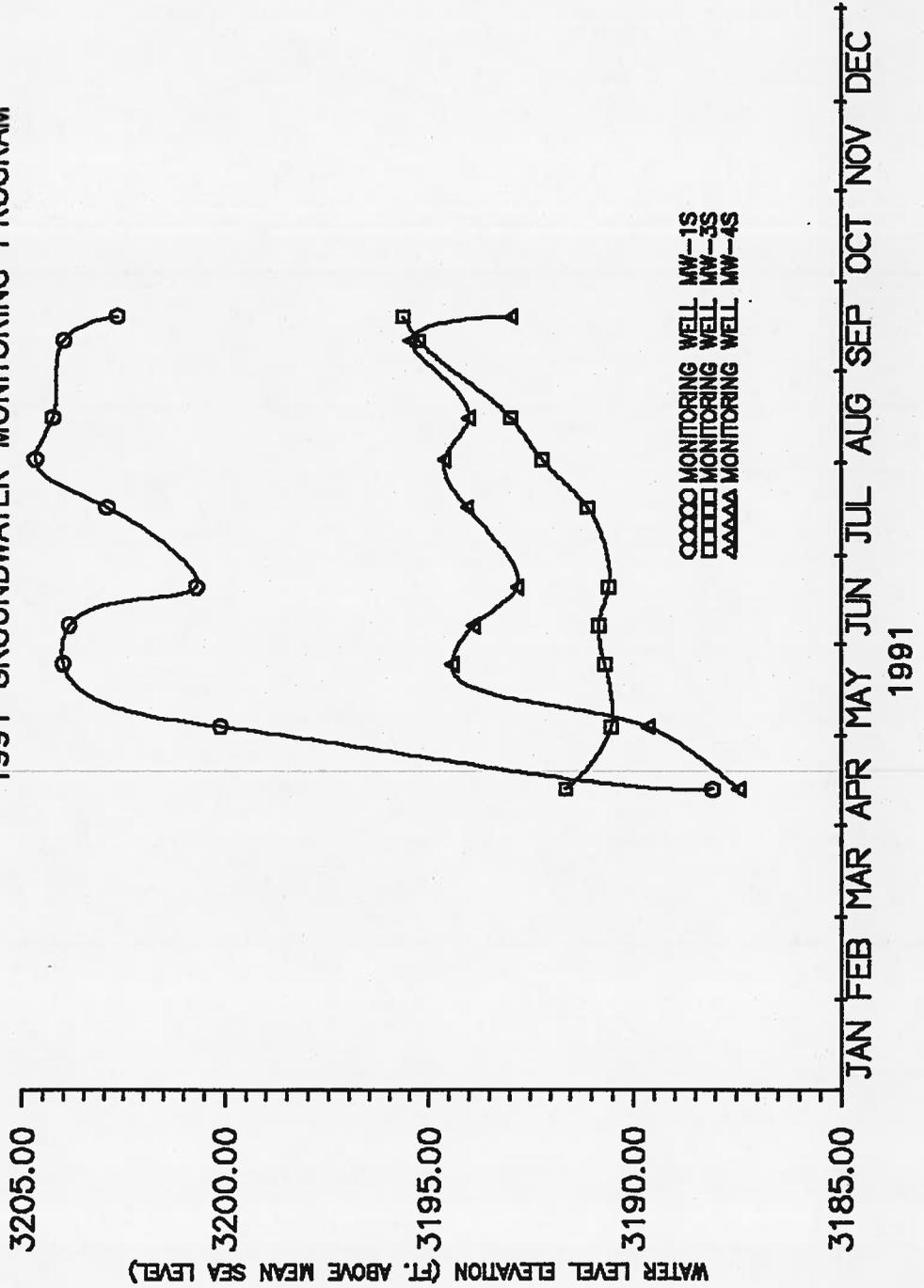


FIGURE 4

HYDROGRAPH OF DEEP MONITORING WELLS
 MW-1D, MW-2, MW-3D AND MW-4D
 1991 GROUNDWATER MONITORING PROGRAM

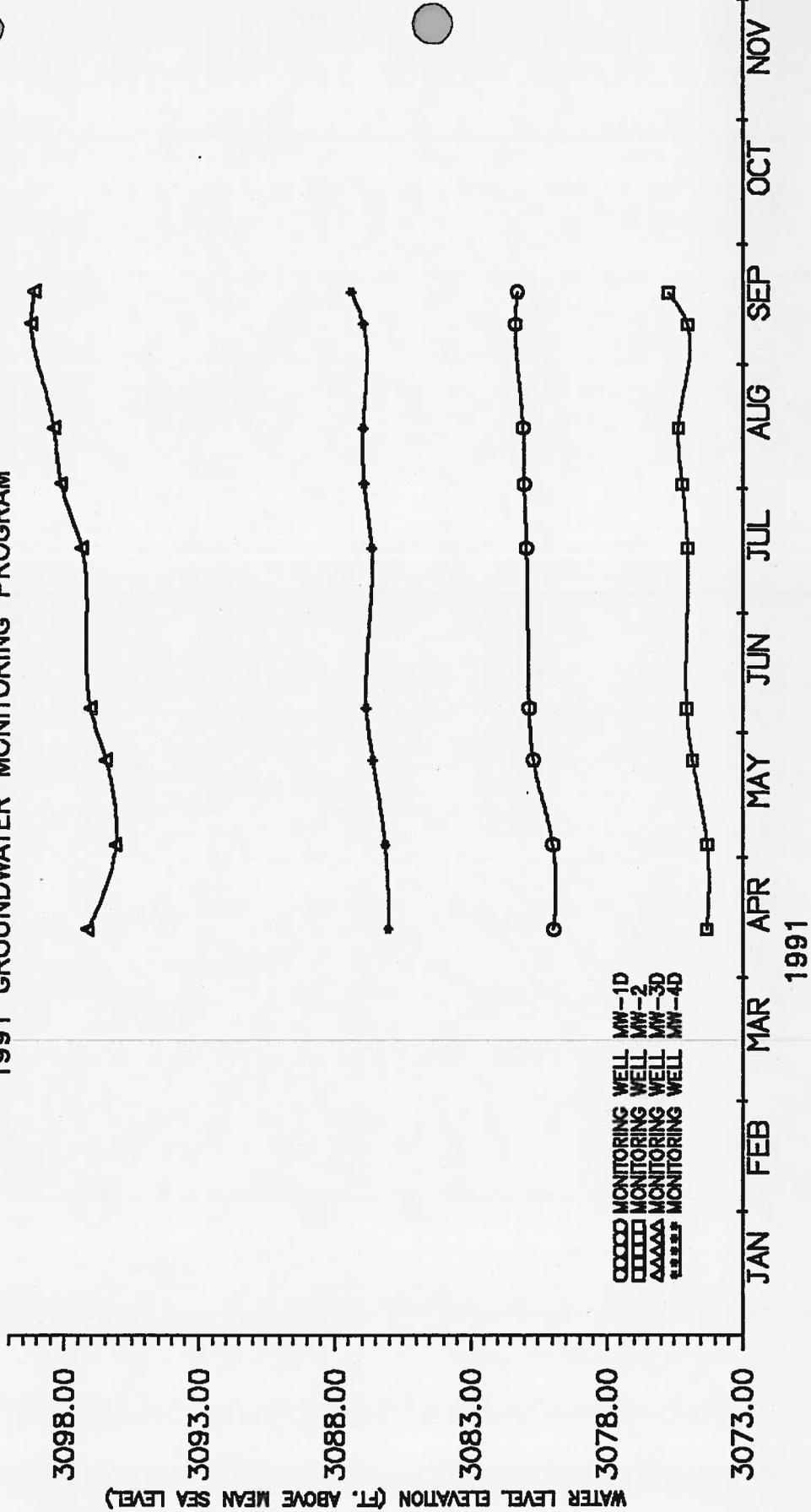


FIGURE 5

On July 9, 1991, MTC, Inc. completed a survey to determine the location of springs and gauging stations. On Figure 2A springs are identified at the highest elevation where water was seen flowing from the talus. In some areas, phreatic plants are found above these elevations. However, surface water could not be positively located due to the coarse talus deposits covering the slope.

Stream discharge rates were measured throughout the period of March to September, 1991. Monitoring stations 5W, 6W, and 7W receive water primarily from spring flows. Monitoring stations 2WU, 2WL, 3W, 4W, and 4WW are influenced by spring flow as well as surface water which drains from the irrigated fields above the basalt escarpment. Stations 1W and 1WW receive water from springs west of the site. Table 2 presents water level information from the spring network. Figure 6 displays discharge fluctuations in springs 5W, 6W, and 7W throughout the period.

3.4 Groundwater Sampling

Water samples were collected from all seven monitoring wells and nine of the measuring stations on April 12, 1991. Sampling followed standard field procedures identified in Appendix B.

3.5 Aquifer Testing

Two types of aquifer tests were completed in conjunction with this investigation; slug tests and pumping tests. The slug tests were performed on July 17, 1991 and were completed by lowering a pressure transducer into the well, allowing the water level to stabilize, and then quickly inserting a solid cylinder into the well causing a sudden water level rise within the well casing. The declining water level was measured on a digital recorder coupled to the pressure transducer.

TABLE 2
Stream Discharge Data
 (all values in cubic feet per second)

<u>Date</u>	<u>Station ID</u>									
	<u>1W</u>	<u>1WW</u>	<u>2WU</u>	<u>2WL</u>	<u>3W</u>	<u>4W</u>	<u>4WW</u>	<u>5W</u>	<u>6W</u>	<u>7W</u>
2-28-91	1.12	NM	0.006	0.006	0.324	0.380	0.266	0.078	0.042	0.072
3-22-91	0.921	NM	NM	NM	0.362	0.424	0.136	NM	NM	0.072
4-03-91	0.973	0.558	0.004	0.004	0.256	0.466	0.103	0.073	0.048	0.080
4-12-91	1.06	NM	0.004	0.004	0.322	0.463	0.071	0.070	0.047	0.080
4-16-91	0.991	1.06	0.004	0.004	0.322	0.463	0.052	0.069	0.047	0.080
4-26-91	1.14	NM	0.004	0.004	0.324	0.468	0.041	0.073	0.049	0.080
5-03-91	1.03	1.39	0.056	0.057	1.03	0.204	0.372	0.070	0.048	0.080
5-11-91	1.01	1.14	0.016	0.016	0.372	0.218	0.076	0.070	0.048	0.080
5-24-91	1.03	1.06	0.035	0.039	0.468	0.226	0.088	0.073	0.052	0.096
5-28-91	1.03	0.73	0.222	0.222	0.854	0.226	0.272	0.070	0.051	0.096
6-06-91	1.14	0.887	0.211	0.225	0.870	0.362	0.539	0.074	0.057	0.096
6-19-91	1.34	0.997	0.099	0.104	0.306	0.515	0.289	0.074	0.062	0.101
7-09-91	0.921	0.921	0.019	0.019	0.382	0.539	0.289	0.069	0.055	0.101
7-16-91	0.887	0.790	0.028	0.029	0.362	0.564	0.272	0.073	0.060	0.096
8-01-91	0.955	0.887	0.047	0.047	0.515	0.240	0.403	0.060	0.059	0.096

TABLE 2 CONT.

<u>Date</u>	<u>1W</u>	<u>1WW</u>	<u>2WU</u>	<u>Station ID</u>						
				<u>2WL</u>	<u>3W</u>	<u>4W</u>	<u>4WW</u>	<u>5W</u>	<u>6W</u>	<u>7W</u>
8-15-91	0.938	0.904	0.022	0.020	0.324	0.539	0.289	0.075	0.063	0.101
9-10-91	1.14	1.10	NM	NM	0.197	0.564	0.324	NM	NM	0.115
9-18-91	1.06	1.06	0.024	0.023	0.272	0.539	0.324	0.092	0.073	0.115

NM - Not Measured

HYDROGRAPH OF SPRING DISCHARGES
 STATION NOS. 5W, 6W, AND 7W
 1991 GROUNDWATER MONITORING PROGRAM

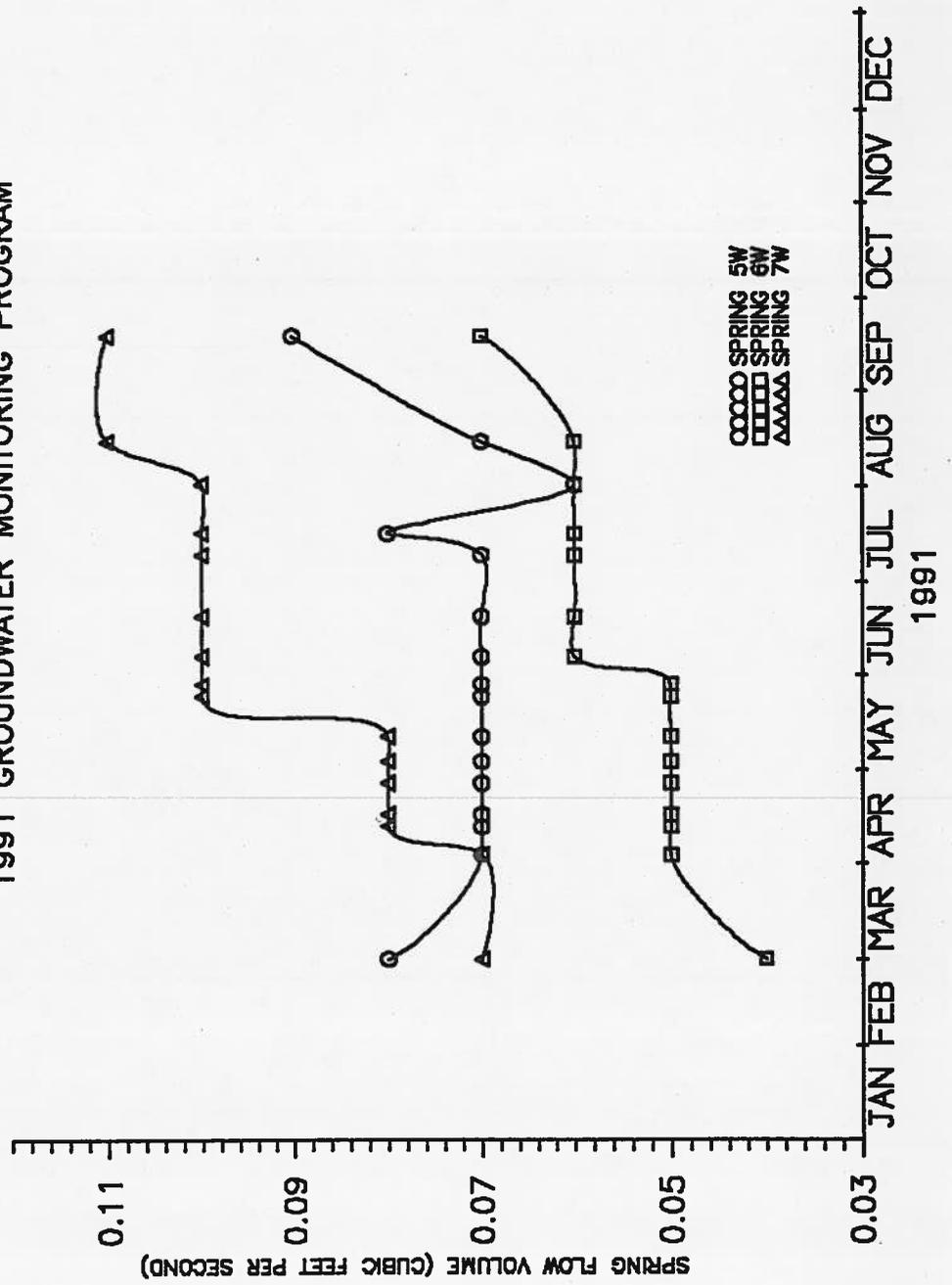


FIGURE 6

The hydraulic conductivity was then calculated using methods described by Bouwer and Rice (1976 and 1989).

A constant discharge test was performed in monitoring well MW-1S on September 10 and 11, 1991. Results from the constant discharge test were used to generate a computer model which estimates groundwater fluctuations due to the construction of the proposed road cut. Appendix E presents details and assumptions used for production of the model.

4.0 LABORATORY ANALYSES

Groundwater samples were submitted to an EPA approved laboratory (Water supply laboratory certificate No. MT-0012) for analysis of cation/anion balance. Appendix B presents complete analytical reports and chain-of-custody documentation. Appendix C summarizes sample handling protocol.

5.0 LOCATION OF WATER WELLS

A well records search was conducted at Idaho Department of Water Resources (IDWR) to identify water wells filed with IDWR that are near the site. Local residents were also interviewed to identify wells not listed in IDWR records. Table 3 presents the owner, depth, water-level, and use of these wells. Figure 7 displays locations of wells within one-half mile of the site.

The majority of wells are located on the plateau area north of the Snake River canyon. Two irrigation wells (Nos. 17 and 18) and one domestic well (No. 19) not registered with IDWR are located approximately one-half mile west of the proposed roadway. A fourth

unregistered well (No. 20), used to water livestock, is present approximately 250 feet east of the alignment and is also identified as Madalena Cellar on Figure 2B. According to Mr. Madalena, all four unregistered wells are completed to depths of about 100 to 120 feet BGS. Appendix C presents copies of well driller reports for registered wells.

6.0 IRRIGATION WATER QUANTITIES

A water rights search was conducted at IDWR to identify sources and quantities of irrigation water currently in use across the site. Additional information was obtained in interviews with the landowner, Mr. Mike Madalena, and Mr. Ted Diehl and Mr. Bob Hackworth, employees of Northside Canal Company.

The land north of the basalt cliffs is irrigated by four major canals. The J8 Canal flows east to west and discharges over the canyon rim approximately one-half mile east of the proposed roadway. Mr. Madalena reportedly diverts and distributes up to 3.5 cubic feet per second (CFS) of water from the J8 canal in a series of secondary ditches which flow intermittently depending on irrigation schedules. Irrigation water not lost through evapotranspiration or infiltration is discharged over the basalt cliff approximately 400 feet south of monitoring well MW-4. The water flows beneath the talus and emerges on the lower slope where it has recently eroded a steep-walled gully about ten feet deep and 100 feet long. The gully trends west to east and intercepts a small spring flow approximately 100 feet west of gauging station 4WW. The water is then channelled by canal past station 4W before discharging into the Snake River approximately one-half mile east of the alignment.

TABLE 3
Water Wells Filed With Idaho Division Of Water Resources
Within 1/2 Mile Of The Site

<u>Reference Number</u>	<u>Owner</u>	<u>Location</u>	<u>Date Drilled</u>	<u>Depth (feet)</u>	<u>SWL (feet)</u>	<u>Screened Interval</u>	<u>Use</u>
1	Mike Madalena	NE of NE Sec.1 T.9S, R.14E	7/81	105	85	open hole below 19 ft.	Domestic
2	John Madalena	SW of SE Sec.36 T.8S, R.14E	3/76	85	70	open hole below 19 ft.	Irrigation
3	Blick	NW of NE Sec.36 T.10S, R.17E	5/70	98	68	open hole below 70'	Irrigation
4	Strickland	NE of NW Sec.31 T.8S, R.15E	7/61	80	59	open hole below 10'	Irrigation
5	North Side Canal Co.	SW of NW Sec.31 T.8S, R.15E	10/76	98	62	open hole below 19.8'	Domestic
6	Neil Ambrose	NW of NW Sec.31 T.8S, R.15E	5/78	105	62	open hole below 19'	Domestic
7	Fleming	NW of NW Sec.31 T.8S, R.15E	6/79	110	75	open hole below 19'	Domestic
8	Northside Farms	NW of NE Sec.31 T.8S, R.15E	4/89	104	70	open hole below 20'	Domestic
9	Frank Henslee	NE of SE Sec.36 T.8S, R.14E	2/68	300	95	unknown	Irrigation
10	Wesley Frizen	SW of SE Sec.1 T.9S, R.14E	9/83	155	110	open hole below 143'	Domestic

TABLE 3 CONT.

<u>Reference Number</u>	<u>Owner</u>	<u>Location</u>	<u>Date Drilled</u>	<u>Depth (feet)</u>	<u>SWL (feet)</u>	<u>Screened Interval</u>	<u>Use</u>
11	O.G. Dairy	SE of SW Sec.36 T.8S, R.14E	6/78	130	80	open hole below 19'	Stock
12	Frank Madalena	SE of SE Sec.31 T.8S, R.15E	4/61	95	unknown	open hole below 70'	Irrigation
13	Ernest Weech	SW of SE Sec.31 T.8S, R.15E	9/51	110	84	open hole below 6'	Irrigation
14	Bill Fleming	SW of SE Sec.31 T.8S, R.15E	4/81	205	90	open hole below 19'	Stock
15	Lee Barnes	NE of NE Sec.12 T.9S, R.14E	3/76	220	86	open hole below 85'	Domestic
16	W. Grissom	NW of NE Sec.36 T.8S, R.14E	5/52	98	72	open hole below 8'	Domestic, Irrigation
Water Wells Not Registered With Idaho Division of Water Resources							
17	John Madalena	SE of SW Sec.36 T.8S, R.14E	unknown	120?	unknown	unknown	Irrigation
18	Melvin Brown	NE of NW Sec.1 T.9S, R.14E	unknown	120?	unknown	unknown	Irrigation
19	Melvin Brown	NE of NW Sec.1 T.9S, R. 14E	unknown	120?	unknown	unknown	Domestic
20	Mike Madalena	NW of NW Sec.6 T.9S, R.15E.	unknown	120?	unknown	unknown	Stock

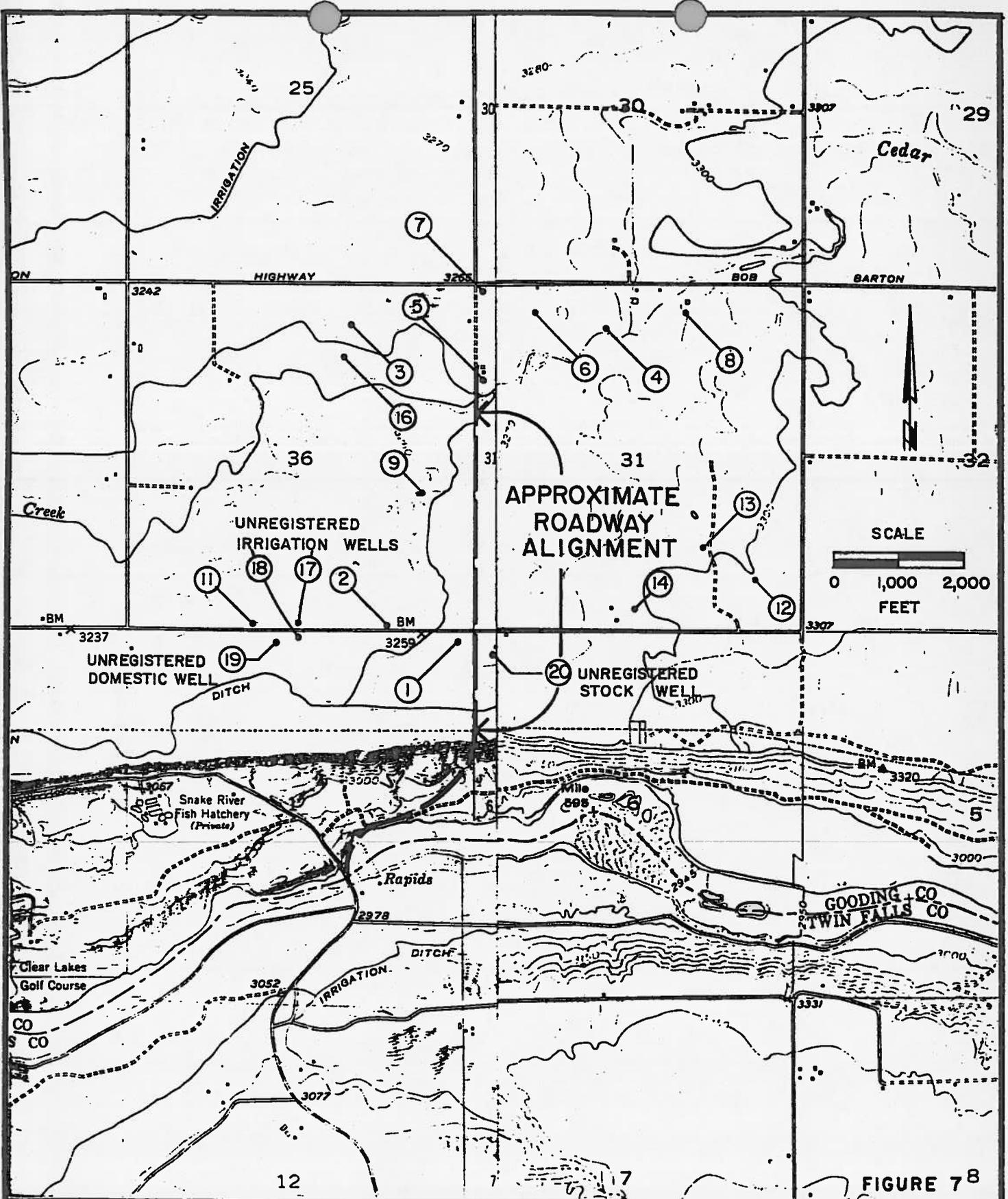


FIGURE 7^B

Chen-Northern, Inc.	LOCATION OF WATER WELLS				IDAHO
	CLEAR LAKES GRADE				
GOODING COUNTY		DRAWN		REVIEWED	
DATE	DRAWN	REVIEWED	SCALE	DRAWING NO.	
SEPT. 1991	JFZ	PTS	AS SHOWN	190-1496	

Three additional unlined irrigation canals flow east to west across the north portion of the alignment. The S Coulee flows across the alignment at station 104 (see Figure 2B) and carries flows of up to 75 CFS (Hackworth, 1991). Less than 1/4 mile east of the site, canal No. S 39 is diverted from S Coulee and crosses the alignment at approximately station 100, flowing south along the west edge of the proposed alignment before turning west at sta. 70 (see Figure 2B). Canal S 39 carries between 12 and 20 CFS. A third canal (S 27) flows at rates of 6 to 12 CFS and is diverted immediately east of the proposed roadway where it crosses at sta. 105. It is significant to note that flows in S39 and S27 are in addition to the 75 CFS in S Coulee.

In the area south of the canyon rim, much of the water flows to the site from the west in an irrigation canal located along the base of the talus slope. Water discharge rates are measured at gauging stations 1WW and 1W. Spring water is added to the canal at stations between 1WW and 1W and at stations 2WU, 2WL and 3W as well as possible other locations not identified in our reconnaissance. Water is collected in a small pond adjacent to 3W and used for irrigation or diverted by 12 inch pipe to a discharge point near the river (see Figure 2A).

7.0 RESULTS AND DISCUSSION

7.1 Local Geology

Lithologic logs from the seven monitoring well borings were used to characterize the subsurface sediments in the northern and central portion of the site. Geologic information from the southern portion of the site was obtained by local geologic reconnaissance. Additional on-site information will be obtained during the geotechnical field investigation phase of the project.

The site is comprised of several distinct geomorphic areas. The southern portion, presently used for alfalfa production, consists of a gently sloping alluvial valley of the Snake River. Surface soils are predominately fine-grained silty sand of alluvial and eolian origin. According to local resident Mr. Madalena, excessive surface water flows periodically produce gullies or circular depressions up to several feet wide in the valley soils.

North of the alluvial valley, the site is steeply sloped to vertical and rises approximately 240 feet in elevation. This portion of the study area includes a nearly vertical basalt escarpment approximately 40 to 80 feet in height which defines the north rim of the Snake River canyon. The basalt is moderately weathered, closely to moderately fractured, finely vesicular, and dark gray to black.

The base of the cliff terminates in talus. The talus slopes southward about 100 to 150 feet in elevation and consists of basalt blocks and boulders up to several feet in diameter. The boulders are subangular to angular, moderately weathered, finely vesicular and dark gray to black. Scattered pockets of phreatic vegetation within the talus suggest shallow surface water, possibly springs which emerge below the boulders.

Below the talus, the terrain is moderately to steeply sloped and covered by fine-grained silty sand. Several small outcrops of basalt are present between spring gauging stations 2WU and 4WW at elevations between 3020 and 3050 feet. The basalt is reddish brown, severely weathered, and closely fractured on exposed surfaces. This area contains the majority of springs on the site and also several gullies and depressions as large as 30 to 40 feet in diameter and 10 feet in depth, presumably formed by excess surface drainage or shallow groundwater flow.

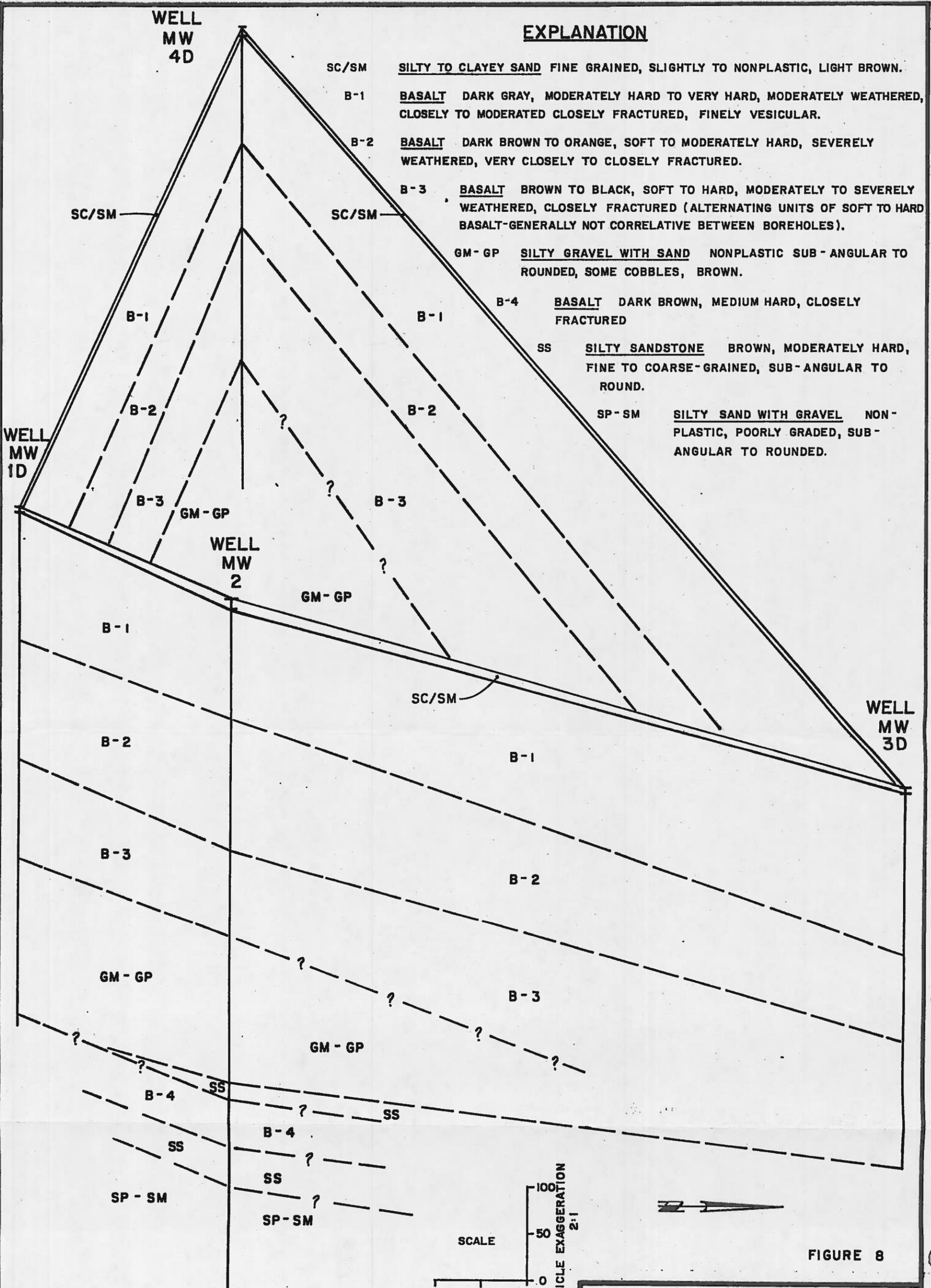
On the basalt plateau north of the canyon rim, the site is covered by 1.5 to 6 feet of silty to clayey sand. The sand is predominately fine grained, slightly plastic, moderately dense to dense and light brown to tan. A small amount of fine gravel and some slightly cemented lenses are present below one foot in depth. The upper six inches of the profile forms topsoil which supports alfalfa and other cattle forage crops.

The surface soils are underlain by several units of basalt bedrock which have been roughly grouped into units B1, B2, B3, and B4, based on general lithologic characteristics which are shown in Figure 8. The upper basalt unit (B1) which is dark grey, hard, moderately weathered, moderately to closely jointed and finely vesicular, extends to approximately 57 to 92 feet BGS and thickens to the north.

The dark gray basalt (B1) is underlain by a series of reddish brown to orange basalt flows (unit B2) which are soft to moderately hard and severely weathered to decomposed. Joints and fractures are very closely to closely spaced and contain moderately plastic clay fillings. During drilling, occasional voids were encountered, resulting in a loss of cuttings for several feet. In some areas, basalt flows are sufficiently weathered to form soil-like lenses. In borehole MW-3D, drill cuttings consisted mainly of clay from approximately 91 to 114 feet BGS.

At depths between about 108 and 138 feet, basalt flows are hard, dark gray to dark brown, vesicular, and moderately weathered (Unit B3). Fractures and joints are closely to moderately spaced, and frequently contain green to blue, slightly indurated clay fillings. Individual flows within this unit vary in thickness from five to eighteen feet.

Basalt units (B1, B2, and B3) are underlain by unconsolidated or lithified sediments below depths ranging from 185 to 205 feet.



NOTE: LITHOLOGIC CONTACTS ARE PRESENTED ONLY TO AID IN VISUALIZATION AND ARE NOT TO BE USED TO INTERPRET ELEVATIONS OF ROCK UNITS OR OTHER FEATURES.

FIGURE 8

GENERALIZED GEOLOGIC FENCE DIAGRAM
CLEAR LAKES GRADE
GOODING COUNTY, IDAHO

Chen-Northern, Inc.

Drawn: JFZ	Scale: AS SHOWN	DRAWING NO.: 190-1496
Checked: PTS	Date: SEPT. 1991	

Across the south portion of the site, the predominant material at this depth consists of silty to sandy gravel which is poorly graded, dense to very dense, subrounded to rounded, and nonplastic with some slightly cemented zones. In the north portion of the study area, basalt unit B3 was underlain by fine to coarse-grained silty sandstone. This sandstone was also encountered in borehole MW-2 beneath the gravel at a depth of about 263 feet to 270 BGS.

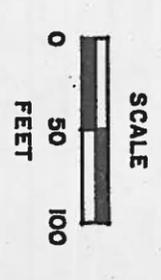
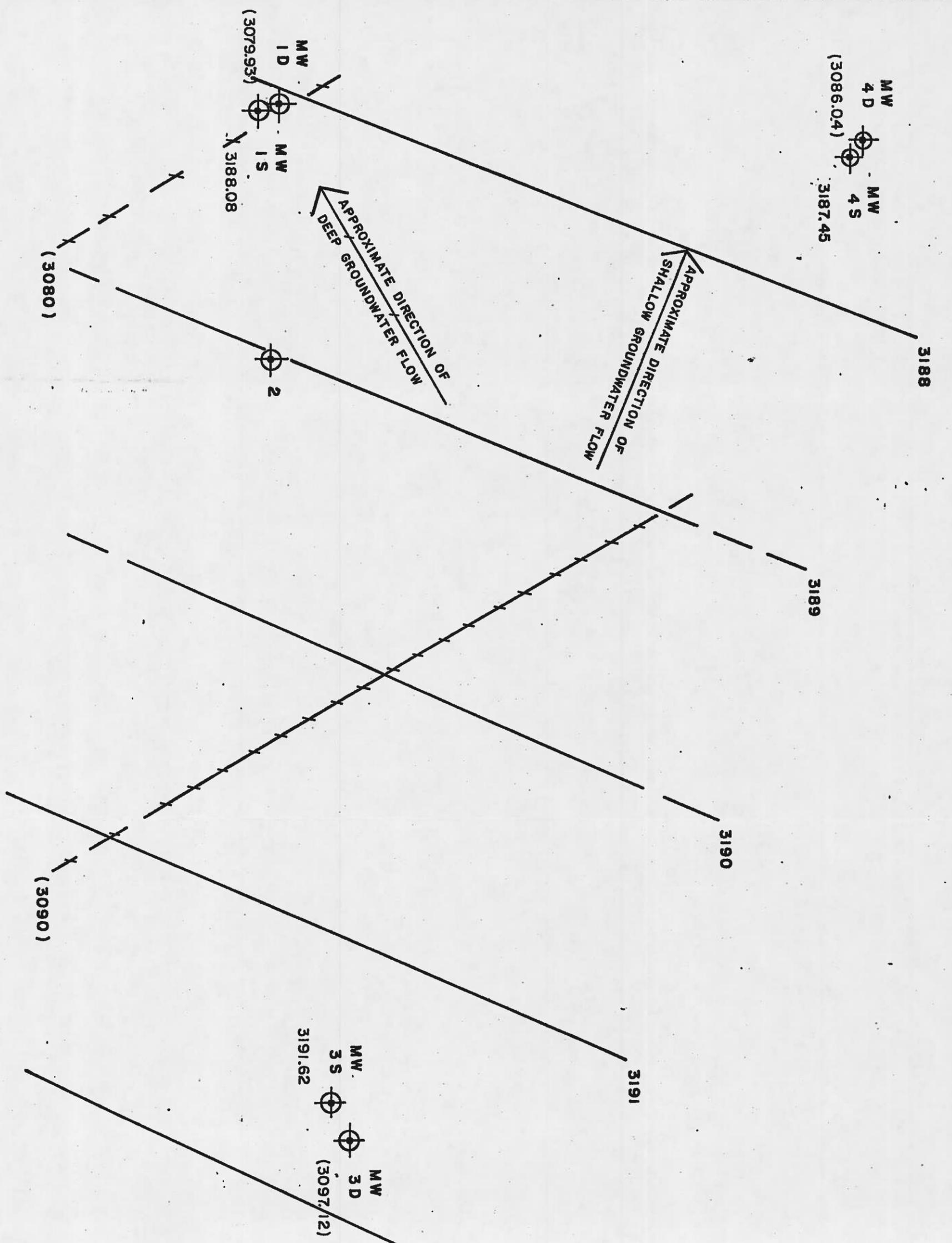
Boring MW-2 was continued to a depth of 400 feet and intercepted basalt (unit B4) or basalt interbedded with sand and gravel from a depth of approximately 270 to 300 feet BGS and silty sand with gravel below 300 feet.

7.2 Hydrogeology

7.2.1 Groundwater Elevations

Static water levels have been measured periodically from April to September, 1991. Measurements indicate the presence of at least two distinct water bearing zones. The upper aquifer is comprised of highly weathered, fractured basalt and contains water at approximately 71 to 92 feet BGS. Water level elevation data indicates that prior to the start of irrigation on April 24, 1991, the groundwater migration direction was towards the southwest with a gradient of about 0.004 (see Figure 9). Since the start of irrigation, water levels have risen five to fifteen feet in Wells MW-1S, MW-3S and MW-4S, probably from surface water recharging the shallow water-bearing unit. As a result, the groundwater flow has shifted to the north-northwest and the gradient has steepened to 0.018 (see Figure 10). Due to the response in water levels to surface irrigation this shallow aquifer appears to be unconfined.

A second aquifer, apparently isolated from the upper unit by low permeability basalt (basalt unit B3), is comprised of unconsolidated to slightly cemented silty to sandy gravel with



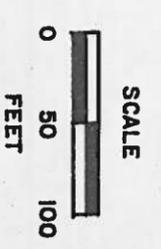
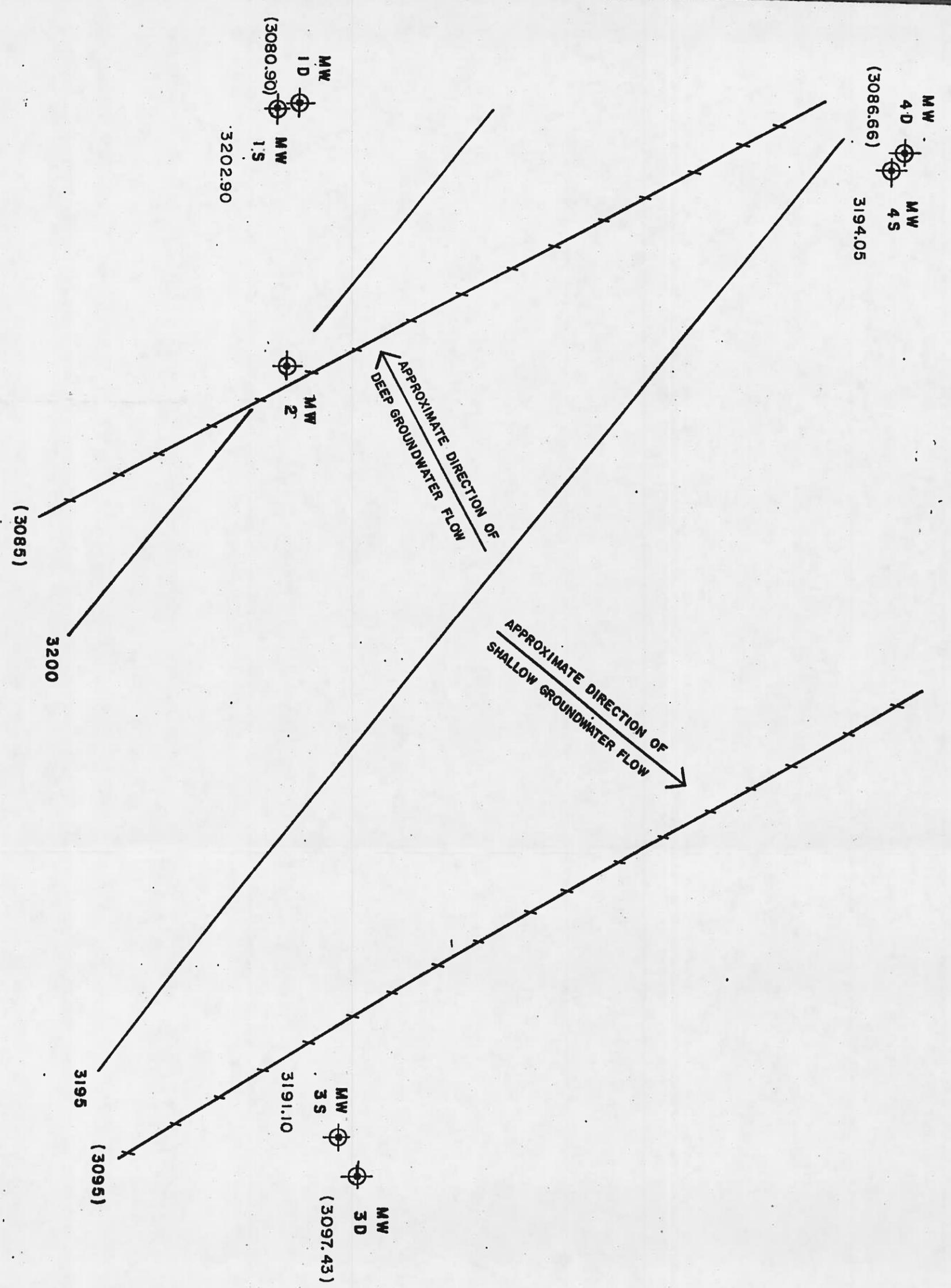
- LEGEND**
- MADALENA DOMESTIC WELL
 - 3192.74
 - 3193
 - MW APPROXIMATE LOCATION OF MONITORING WELL
 - 3191.62 WATER LEVEL IN SHALLOW WELL
 - (3097.12) WATER LEVEL IN DEEP WELL
 - (3097.12) WATER LEVEL CONTOUR IN SHALLOW WELL
 - WATER LEVEL CONTOUR IN DEEP WELL

FIGURE 9

WATER TABLE MAP
 (MEASURED 4-12-91)
 CLEAR LAKES GRADE
 GOODING COUNTY,
 IDAHO

Chen-Northern, Inc.

Drawn	JFZ	Scale AS SHOWN	DRAWING NO.:
Checked	PTS	Date: SEPT. 1991	190-1496



- LEGEND**
- MW APPROXIMATE LOCATION OF MONITORING WELL
 - WATER LEVEL IN SHALLOW WELL
 - WATER LEVEL IN DEEP WELL
 - WATER LEVEL CONTOUR IN SHALLOW WELL
 - WATER LEVEL CONTOUR IN DEEP WELL

FIGURE 10

WATER TABLE MAP
(MEASURED 7-16-91)
CLEAR LAKES GRADE
GOODING COUNTY, IDAHO

Chen-Northern, Inc.

Drawn:	JFZ	Scale:	AS SHOWN	DRAWING NO.:
Checked:	PTS	Date:	SEPT. 1991	190-1496

groundwater encountered at depths from 185 to 200 feet BGS. The groundwater migration direction is generally to the south with an average gradient of 0.019. Water levels in the lower aquifer are not significantly affected by irrigation practices, as evidenced by the relative stability of measurements throughout the monitoring period. This suggests the aquifer is possibly confined.

Water levels in monitoring well MW-2, screened in unconsolidated gravel between 230 and 250 BGS, have consistently remained approximately 5 feet lower than water levels observed in MW-1D, MW-3D, and MW-4D. This deeper water-bearing zone is apparently confined and separated from the overlying aquifer, perhaps by lithified sedimentary layers.

7.2.2 Aquifer Performance Tests

Slug tests, performed on wells MW-2 and MW-3D on July 16, 1991, indicated hydraulic conductivities ranging from about 1 foot per day (ft/day) in monitoring well MW-2 to .5 ft/day in well MW-3D.

Slug tests provide estimates of hydraulic conductivity in the area immediately surrounding a well, but in fractured bedrock conductivity values are highly variable due to the fracture patterns in the rock. Hydraulic conductivities in well developed fracture zones may be several orders of magnitude higher than that observed in unfractured areas. Other anisotropies, such as variations in lithology, weathering or cementation may also cause significant differences in conductivity measurements.

Aquifer performance tests pump a known quantity of water from one well while water level fluctuations are measured in surrounding wells. These tests are more reliable indicators of aquifer conditions because the area between a pumping well and an observation well is used to calculate hydraulic conductivity.

In this regard, a pump test was performed on monitoring well MW-1S on September 10 and 11, 1991. The well was pumped with a 3 horsepower submersible pump at a constant rate of 7 gallons per minute for a period of approximately 25 hours. Water levels were periodically measured in wells MW-4S, MW-1S, MW-1D and exploratory boring B-1. The pumping rate was monitored throughout the test using a stop-watch and five gallon bucket. Water level fluctuations were recorded in well MW-4S, located approximately 550 feet west of MW-1S, and in exploratory boring B1, situated in the proposed road cut fill area 280 feet east of MW-1S. In the test area, hydraulic conductivities ranged from about 5 ft/day between MW-1S and MW-4S, to 3.5 ft/day between MW-1S and B1. Appendix D presents a summary of slug test data and pump test results from the monitoring well network.

7.2.3 Estimated Effects of Construction Activities

During and after construction, the deep cut at the canyon rim will intercept groundwater from the shallow unconfined aquifer. A drainage plan will be required to remove the water encountered. Based on the current roadway profile supplied by Sharp and Smith, a computer model was run to estimate the quantity of water which would flow from the road cut during the irrigation season. Using a hydraulic conductivity of 5 ft/day, a flow of 0.03 CFS would be predicted, once the aquifer had attained steady-state conditions. During the irrigation season, water levels are at seasonal highs. As water levels decline in the winter months, the flow from the road cut should decrease.

The observed conductivity produced from pump test data was then compared with a range of literature values reported for fractured basalt (Freeze and Cherry, 1979). Literature values ranged from 0.02 ft/day to 220 ft/day, placing observed site conditions in the approximate middle range of values. A second computer model was run using a "worst case" conductivity of 150 ft/day. Using the

textbook value, a steady state flow rate of 1 CFS from the road cut was generated. Use of this elevated figure should account for anisotropic variations not measured in the pump test.

Potentially significant elements not included in this analysis and modelling effort relate to increased hydraulic conductivity at the road cut due to blasting and mass removal (load relaxation) resulting in widening of existing fractures at the road cut face, lateral increases in hydraulic conductivity from that measured during the pump test, effects of drought over the last five years on "normal" water levels versus those measured, and flushing of sediment from fractures at the road cut face. Accounting for these factors and using a safety factor of 10 times, a reasonable flow rate from the road cut for conveyance design may be 0.5 CFS.

It is expected that construction of the road cut will be completed over the course of weeks to months. At this rate, drainage of groundwater levels should not exceed the value predicted by the computer model. If the road cut is completed at faster rates, flows exceeding the predicted value may occur.

A second area of consideration concerns effects on shallow wells and springs near the proposed roadway cut. Drainage of the shallow aquifer by the cut will cause a depression in the surrounding water table. Based on computer models, the zone of influence from the road cut will extend to the north, east and west approximately 2,000 feet. Water levels will decline approximately one foot in the Madalena domestic and cellar water wells (well Nos. 19 and 20), located about 1,400 feet north of the road cut. Other wells in the vicinity should be largely unaffected by water loss. Figure 11 depicts a theoretical model of water level elevations in the shallow aquifer prior to and following roadway construction.

Another area of concern to local water wells is the effect of blasting on the sidewalls of the wells. The wells in the vicinity

of the construction area are typically uncased. Blasting may cause some rock displacement within the well annulus, resulting in damage to down-hole pumping equipment. The Madalena domestic well is located approximately 60 feet west of a potential blast area, while the Madalena cellar well is situated about 380 feet east.

Although quantitative information is not available, it is anticipated that spring flow in the area immediately below the cut may be reduced. However, any decrease would be offset by drainage from the cut. Assuming a radius of influence of 2,000 feet, the large springs which provide water for Clear Lakes Fish Hatchery, located over 6,000 feet west of the cut, should not be affected.

Groundwater from the deeper aquifers is not expected to significantly affect roadway construction activities. The elevation of the top of the lower aquifer ranges from 3,080 to 3,100 feet above mean sea-level and the bottom of the road cut is anticipated at an elevation of 3,165 feet, based on road profile information provided by Sharp and Smith.

7.2.4 Surface Water

During the irrigation season, an overland flow of up to three and one half CFS is distributed over the area surrounding the proposed road cut, as estimated by Mr. Madalena. In addition, irrigation canals S Coulee, S 39 and S 27, in the north portion of the project, flow at rates of 75, 20 and 12 CFS, respectively. There are no perennial streams or significant natural drainages north of the canyon rim.

In the area below the cliff, a perennial stream located at the toe of the talus slope flows from the existing roadway to the small collection pond south of stream gauge 3W. The water is currently piped from the collection pond south below the proposed roadway through a twelve inch iron pipe to a discharge port near the Snake

River (Figure 2). Cumulative water measurements obtained from gauging stations 1W, 2WL, and 3W indicate a discharge rate ranging from 1.3 CFS on April 3, 1991 to 2.5 CFS on May 3, 1991. Some water also flows parallel to the existing road and is stored in a marsh located near the south end of the proposed roadway between stations 26+50 and 28+50. Drainage plans may need to be considered for the marsh. Federal and State regulations should be considered to determine if they apply.

A second stream begins west of gauging station 4WW and flows west to east along the base of the slope and discharges into the Snake River approximately one-half mile east of the site. Cumulative measurements from stations 4WW, 4W, 5W, 6W and 7W suggest a flow rate ranging from 0.5 to 1.1 CFS.

7.3 Field and Analytical Test Results

Table 4 presents a summary of groundwater field measurements. In general, specific conductance values were higher in MW-1S, MW-3S and MW-4S and MW-2 than wells MW-1D, MW-3D and MW-4D. The pH in MW-2 was notably higher than other well samples.

TABLE 4

Summary of Groundwater Field Measurements

<u>Sample Location</u>	<u>Date Sampled</u>	<u>pH</u>	<u>Temperature (°C)</u>	<u>Specific Conductance (umhos (cm.))</u>
MW-1S	4-12-91	7.55	13.8	732
MW-1D	4-12-91	7.62	13.4	559
MW-2	4-12-91	8.07	13.5	684
MW-3S	4-12-91	7.49	13.3	694
MW-3D	4-12-91	7.55	13.0	583
MW-4S	4-12-91	7.64	13.2	655

TABLE 4 CONT.

<u>Sample Location</u>	<u>Date Sampled</u>	<u>pH</u>	<u>Temperature (°C)</u>	<u>Specific Conductance (umhos (cm.))</u>
MW-4D	4-12-91	7.62	12.2	517
1W	4-12-91	NA	16.0	589
2WU	4-12-91	NA	13.3	671
2WL	4-12-91	8.08	14.3	654
3W	4-12-91	7.90	16.2	601
4W	4-12-91	7.91	15.8	574
4WW	4-12-91	7.91	15.6	593
5W	4-12-91	7.94	15.7	581
6W	4-12-91	7.90	14.8	570
7W	4-12-91	7.89	15.0	584

NA - Not Analyzed

Field samples obtained from the stream gauging network indicate pH values similar to MW-2. Specific conductance values are most correlative to MW-1D, MW-3D and MW-4D.

Table 5 presents a summary of analytical results of water samples collected from all seven monitoring wells and nine of the gauging stations. Calcium carbonate alkalinity was generally greater than 200 milligrams per liter (mg/l) in the shallow wells and less than 200 mg/l in wells MW-1D, MW-3D and MW-4D. Monitoring well MW-2 apparently differs from the other deep wells as evidenced by an elevated sulfate value (67 mg/l) and lower calcium and magnesium concentrations (24 and 10 mg/l).

Water samples from stream gauging stations 4W, 5W, 6W, and 7W showed a general uniformity. Differences in 1W, 2WU, 2WL, and 3W could be attributed to surface water which is transported from west of the site.

Spring samples are similar but not strongly correlative with the well samples and may indicate a combined flow contribution from several aquifers as well as surface water. Appendix E presents complete analytical test reports and chain-of-custody documentation.

8.0 RECOMMENDATIONS

During the preliminary design phase of the project, a number of considerations should be evaluated to minimize hydrologic impacts. In the north portion of the roadway, water from irrigation canals S 27, S 39 and S Coulee will need to be channeled under the road. According to Northside Canal Company personnel, as much as 107 CFS of water may be present in the three canals.

In the area south of the Madalena residence (see Figure 2A), the current landholder is diverting 3.5 CFS onto fields for irrigation. Much of this water will intercept the east side of the future road cut and will need to be routed to the west side of the cut or be otherwise accounted for in drainage considerations.

TABLE 5
Summary of Analytical Results of Water Samples
 Date Sampled 4-12-91

Sample Location	Anions				Total Alkalinity as CaCO ₃	Cations			Nutrients & Nitrate & Nitrite as N		
	Chloride as Cl	Fluoride as F	Sulfate as SO ₄			Calcium as Ca	Magnesium as Mg	Potassium as K	Sodium as Na	Nitrate	Nitrite
MW-1S	29	0.93	41		258	51	22	6.6	46	0.99	
MW-1D	42	0.49	53		154	47	17	7.5	27	1.47	
MW-2	55	0.58	67		186	24	10	5.2	108	1.71	
MW-3S	40	0.55	44		198	51	24	6.7	35	2.86	
MW-3D	40	0.55	49		179	56	22	6.5	29	2.24	
MW-4S	27	0.53	57		246	60	23	6.3	46	0.94	
MW-4D	38	0.53	40		159	45	16	7.3	33	1.79	
1W	38	0.53	25		161	45	19	4.3	25	1.44	
2WU	36	0.78	37		213	47	26	4.6	33	1.17	
3W	40	0.53	40		164	45	19	4.6	25	1.41	
4W	40	0.53	47		161	54	21	4.4	30	1.37	
5W	39	0.58	52		171	55	21	4.3	30	1.30	
6W	37	0.55	52		159	53	21	4.3	29	1.31	
7W	38	0.58	46		166	53	21	4.4	29	1.30	

(all concentrations are expressed as milligrams per liter which is equivalent to parts per million)

The road cut will intercept the upper aquifer along the north rim of the canyon resulting in a local depression in the water table and drainage of groundwater. Based on computer modeling, the groundwater discharge will most likely range from 0.03 to 1 CFS based on water levels observed during the irrigation season. Plans should be made to divert this water, presumably downgrade towards the river. Drawdown effects on local domestic and irrigation wells should be minimal with approximately one foot of loss in the Madalena domestic well and only minimal effect beyond the radius of influence of 2,000 feet. Blasting during construction may cause additional damage due to side wall failures in uncased wells.

Although conservative literature estimates have been used to predict groundwater flow from the road cut, it is possible that unanticipated subsurface conditions could be present which would increase the volume of water released. Diligent efforts have been made to allow for all variables, but a preferable method of forecasting water volumes would be to install an array of large volume pumping wells, completed such that the entire volume of the road cut could be de-watered prior to construction. In this manner, the actual volume of water could be measured under steady state conditions.

In addition, construction activities will also potentially affect local groundwater flow. The area surrounding the cut will be relatively more fractured, due to blasting. Fractures which presently contain soil fillings will likely be flushed clean, resulting in potentially higher flow rates. We recommend that upon completion of the cut, additional measurements be completed on water flow from the cut to assure adequate drainage structures are constructed.

The section of road south of the canyon rim will require drainage measures to divert spring flows and surface water from the north to the south of the fill. The channel which flows from gauging

station 1WW to 3W has contained between 1.3 and 2.5 CFS throughout the measuring period. Due to the large surface area upgradient of this channel, flows could exceed 2.5 CFS during severe storm events. The channel flowing from gauging station 4WW to 7W has carried from 0.5 to 1.1 CFS and lies directly under the proposed fill area. In addition, numerous springs daylight under the proposed fill. Construction activities in this area may yield additional springs not presently identified, and thus increase the amount of surface water.

One buried water source, located in the vicinity of the proposed fill slope, discharges from a six-inch pipe located in the south portion of the irrigated field below the talus slope (See Figure 2A). According to Mr. Madalena, the spring is encased in a box and piped to the discharge point near the Snake River. We recommend that the spring box be located to assure that it will not adversely affect the roadway in the future.

The marsh near the south end of the project contains water from springs west of the present roadway. In the event of high water flows from storm events or spring runoff, plans should include a method of dewatering the marsh and routing excess water across the new road.

9.0 SUMMARY

The northern portion of the site consists of 1.5 to 6 feet of silty sand soil covering a series of basaltic lava flows to depths ranging from 185 to 205 feet BGS. The upper basalt (unit B1) is dark gray, moderately weathered, moderately closely fractured and finely vesicular. A severely weathered, dark brown to orange, water bearing basalt (unit B2) underlies the gray basalt to depths

of 108 to 132 feet BGS. The weathered basalt is underlain by moderately weathered brown to black basalt (unit B3).

The basalt units overlie a sedimentary unit which persists to the depths drilled, approximately 400 feet, although minor flows of basalt may be present between 270 and 300 feet BGS. Near the canyon rim, silty gravel with sand occurred to about 260 feet BGS. In MW-3D to the north, a fine to coarse grained sandstone was present below 205 feet. A lens of basalt approximately 20 feet in thickness was identified in MW-1D below 276 feet (unit B4). Black drill cuttings obtained from MW-2 at a similar depth also suggest a thin basalt bed. Boring MW-2 continued through sandstone and silty gravel units to 400 feet BGS.

Groundwater is present below the site in several different aquifers. A perched shallow aquifer comprised of weathered and fractured basalt is found at 71 to 92 feet BGS. The water flow direction prior to the start of irrigation was to the southwest at a gradient of 0.004. Since irrigation began on April 24, 1991, the flow direction has shifted to the north-northwest with a gradient of 0.018. Hydraulic conductivities measured in the shallow aquifer ranged from 3.5 to 5 ft/day.

A lower, confined aquifer consisting of silty to sandy gravel was encountered at depths ranging from 185 to 197 feet BGS. Since April, 1991, the groundwater flow direction has remained southerly with a gradient of 0.019. Slug tests performed in July, 1991, indicate a hydraulic conductivity of about 0.5 ft/day. A third, apparently confined water bearing unit may be located at approximately 230 feet BGS.

A review of area well driller reports indicate several water wells are located within one-half mile of the site. The majority of wells are located in the shallow aquifer on the plateau north of the Snake River canyon and are used for irrigation or domestic

purposes. Some drawdown in wells located within approximately 2,000 feet of the road cut may be experienced due to depression of groundwater surrounding the cut. Based on computer modeling and the profile supplied by Sharp and Smith, the Madalena domestic and cellar wells may lose about one foot of static water level elevation due to the proposed road cut dewatering.

Road construction should be largely unaffected by groundwater on portions completed at approximate existing grade. Work in the cut section of roadway will need to include a drainage plan to remove approximately 0.03 to 1 CFS flowing from the cut slopes. Based on a safety factor of ten times the calculated flow rate, and accounting for other potentially significant factors, a flow rate of 0.5 CFS may be reasonable for preliminary design of water conveyance structures in the road cut.

Drainage structures will be necessary to allow as much as 3 to 5 CFS of spring and surface water to migrate beneath the fill slopes of the project at the base of the canyon rim. Additional water may be introduced by the cut slope above the fill.

Springs in the area of construction may experience a drop in flow rate, depending on the contribution supplied by the shallow aquifer to total spring flow. Springs in the area of Clear Lakes Trout Hatchery will not be influenced by construction activities, based on the information collected to this date.

It is important to point out that numerous factors can influence the hydrologic regime of a fractured basalt aquifer, especially in the Clear Lakes area. The lateral continuity of the aquifer is uncertain, which may result in conditions substantially different than those calculated during this investigation. However, the general lack of large-volume spring flows (similar to those west of the site near the fish hatchery) in the immediate vicinity of the proposed road cut tends to support aquifer parameter data collected

during this investigation. Other factors of note include the effects of drought conditions on the aquifer as evaluated during this investigation. Also, additional surface run-off that may occur during certain precipitation events, such as rain-on-snow, could impact drainage control structures.

Prepared By: Paul T. Spillers
Paul T. Spillers
Staff Geologist

Reviewed By: Paul K. Hunter
Paul K. Hunter
Hydrogeologist

Roger E. Braun
Roger E. Braun
Senior Hydrologist

10.0 REFERENCES CITED

- Bouwer, H., 1989, The Bouwer and Rice Slug Test - An Update, Groundwater, Vol. 27, No. 3, pp 304-309.
- Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells, Water Resources Research, v. 12, pp. 423-428.
- Diehl, T., 1991, Personal Communication
- Freeze, R.A., and Cherry, J.A., 1979, Groundwater, Prentice Hall Inc., Englewood Cliffs, New Jersey.
- Goodman, R.E., Introduction to Rock Mechanics, 1980, John Wiley & Sons, New York.
- IDHW, 1985, Snake Plain Aquifer Technical Report, 117 pp.
- Madalena, M., 1991, Personal Communication.
- Malde, H.E. and Powers, H.A., 1962, Upper Cenozoic Stratigraphy of Western Snake River Plain, Idaho, Geological Society of America, Vol. 73, p. 1197, October, 1962.
- Malde, H.E. and Powers, H.A., 1972, Geologic Map of the Glenns Ferry-Hagerman Area, West Central Snake River Plain.
- McDonald, M.G. and Harbaugh, A.W., 1988, A Modular Three-Dimensional Groundwater Flow Model, United States Geological Survey, Open-file Report 83-875.
- Street, L.V., and DeTar, R.E., 1987, Geothermal Resource Analysis in Twin Falls County, Idaho Department of Water Resources Water Information Bulletin No. 30 Part 15, 42 p.
- Thomas, C.A., 1968, Records of North-Side Springs and Other Inflow to Snake River between Milner and King Hill, Idaho, 1948-67, Idaho Department of Reclamation, Water Information Bulletin No. 6.

APPENDIX A

**Lithologic Logs
Classification Methods
Monitoring Well Completion Details**

Representative samples were collected from drill cuttings at approximately five to ten-foot intervals. Routine field subsoil and rock classification procedures were performed during drilling. Classification of unconsolidated material consisted of visual and textural identification in accordance with ASTM D2487, which is based on the Unified Soil Classification System. The rock identification procedure was modified from R. E. Goodman (1980).

Monitoring wells were installed in each boring using threaded, flush joint 4-inch I.D. schedule 40 PVC casing. A 20 to 25 foot section of manufactured screen with 0.02 inch openings (No. 20 slot) was installed in each boring. Washed 1/4 inch drain rock was placed in the annular space over the entire screened interval. Granular bentonite was backfilled above the drain rock to within approximately 6 feet below ground surface (BGS). A 6 inch diameter, above ground steel well protector with locking cap was concreted over the borehole to prevent surface contamination and unauthorized access. Tight fitting well caps were placed on the well casings.

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-1S

LEGAL LOCATION: T9S R14E S1 TRACTSE 1/4 NE 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 3-26-91 DATE COMPLETED: 3-27-91 DRILLING COMPANY/DRILLER: Walker Water Systems/F. Walker LOGGED BY: R.J. Pederson

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water

TOTAL DEPTH DRILLED (ft): 105 TOTAL DEPTH CASED (ft): 105 INTERVAL PERFORATED from: 80 to: 100 DIAMETER OF CASING: 4" TYPE OF CASING: Sch 40 PVC

METHOD OF PERFORATION: Open Hole Open Bottom Saw Slotted Factory 0.020 (size) OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE: YES NO
 WELL DEVELOPED
 WELL PUMPED
 WATER SAMPLES COLLECTED
 MATERIAL SAMPLES COLLECTED

ANNULAR COMPLETION CHARACTERISTICS
 WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: Concrete from: 0 to: 6.6'
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 6.6' to: 60'
 FILTER PACK: Type: 1/4"Gravel/Sand from: 60' to: 105'

STATIC WATER LEVEL FT: 88.83' MEASURING POINT DATE: 3-28-91 DESCRIPTION/ ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +1.26

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0	Silty SAND with Minor Clay; slightly plastic, fine grained, tan, (SM)	0-10'	0.5 ft/min
3.0	BASALT; dark brown to dark grey, hard, close spaced fractures, moderately weathered, vesicular, fine grained, less weathered and wide spaced fractures beginning at 9.5' BGS, dark brown	10-15'	0.8 ft/min
		15-20'	0.7
		20-30'	0.4
16.5	BASALT; dark grey, moderately hard, moderately close spaced fractures, fresh, vesicular, fine grained	30-40'	0.6
	- rock softer at 61' (close spaced fractures)	40-50'	0.8
	- 61-64.8' moderately close to widely spaced fractures	50-60'	1 ft/min
	- 64.8-69.1' close spaced fractures	60-70'	0.7 ft/min
69.1	BASALT; medium brown, medium hard to soft, close spaced fractures, moderately to severely weathered, vesicular	70-80'	2 ft/min
		80-90'	0.8 ft/min
		90-95'	0.8 ft/min
105	Bottom of Hole	95-105'	0.7 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-1D

LEGAL LOCATION: T9S R14E S1 TRACTNE 1/4 NE 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 3-25-91 DATE COMPLETED: 3-26-91 DRILLING COMPANY/DRILLER: Walker Water Systems/F. Walker LOGGED BY: R.J. Pederson

DRILLING METHOD: Air Rotary DH Hammer BOREHOLE DIAMETER (in): 8" DRILL FLUIDS USED: Water and Quick Foam

TOTAL DEPTH DRILLED (ft): 280 TOTAL DEPTH CASED (ft): 207.5 INTERVAL PERFORATED from: 182 to: 207 DIAMETER OF CASING: 4" Sch 40 TYPE OF CASING: PVC (Aardvark)

METHOD OF PERFORATION: Open Hole Open Bottom Saw Slotted Factory 0.020 (size) OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE:

	YES	NO
WELL DEVELOPED	<input type="checkbox"/>	<input checked="" type="checkbox"/>
WELL PUMPED	<input type="checkbox"/>	<input checked="" type="checkbox"/>
WATER SAMPLES COLLECTED	<input type="checkbox"/>	<input checked="" type="checkbox"/>
MATERIAL SAMPLES COLLECTED	<input checked="" type="checkbox"/>	<input type="checkbox"/>

ANNUAL COMPLETION CHARACTERISTICS

WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: Concrete from: 0 to: 6'

LOCK NO.: Dolphin 1600 BACKFILL: Material: Bentonite from: 6' to: 164'

FILTER PACK: Type: 1/4" Washed Gravel from: 164' to: 207'

STATIC WATER LEVEL FT: 196.92 MEASURING POINT DATE: 3-28-91 DESCRIPTION/ ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +0.95

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0 - 0.5	TOPSOIL, Silty SAND; fine to medium grained with moderate organic matter		
0.5	Silty SAND; slightly indurated, minor clayey laminae, nonplastic, medium to dark grey, becoming more clayey downward, sandier zones are more strongly cemented (SM)	1.5-6.5'	1 ft/min
1.5	BASALT; dark grey to dark brown, moderately hard to hard, minor vesicles, becomes harder and brown at 9.5' BGS	6.5-9.5'	1.6 ft/min
11	BASALT; medium to dark grey, hard, slightly vesicular, minor clay or alkali salt coatings on fracture surfaces	10-15'	1.2 ft/min
31.2	Well Fractured BASALT	15-30'	1 ft/min
33.1	Hard BASALT; dark brown to dark grey	30-40'	0.8 ft/min
54.0 - 54.3	Void: abundant fractures at 61.2'	40-50'	0.8 ft/min
		50-60'	1.7 ft/min
71.3	BASALT; brown, weathered with close-spaced fractures, very fine grained, minor clay on fractures, alkali salts on vesicles, zone is water saturated	60-70'	1.7 ft/min

JOB NO.: 190-1496

PROJECT: Clear Lakes GradeWELL NO.: MW-1D

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
101	BASALT; dark brown, medium hard, abundant close spaced fractures, heavily weathered, locally contains clay, vesicular, very fine grained, becomes softer and increasing clay downward to 116.5'	70-80'	2 ft/min
		80-90'	2 ft/min
		90-100'	2 ft/min
		100-110'	1 ft/min
116.5	BASALT; dark brown, hard, wide spaced fractures with tan and green blue clay fillings, fresh fine grained basalt with minor vesicles	110-120'	.5 ft/min
		120-130'	.5 ft/min
137	BASALT; dark grey, very hard, wide spaced fractures, minor vesicles	130-140'	.6 ft/min
		140-150'	.5 ft/min
150.8	BASALT; dark grey to medium brown, medium hard, close spaced fractures, vesicular	150-160'	.8 ft/min
		160-170'	.8 ft/min
178.6	BASALT; dark to medium brown, medium hard, close spaced fractures becoming more altered, softer, and light brown downward	170-180'	.4 ft/min
		180-190'	1 ft/min
191	Silty GRAVEL with Sand; soft, round to subround, fine grained, light brown, weakly cemented in zones, tan to medium brown (GM/GP)	190-200'	2 ft/min
		200-210'	2 ft/min
210	Sandy GRAVEL with Silt; soft, round to subround, medium to very coarse sand, subround, saturated, tan (GP)	210-220'	1.4 ft/min
	Resumed drilling on 3-26-91	220-230'	1.4 ft/min .
240	Poorly Graded GRAVEL with Minor Coarse to Very Coarse Sand; round to subround, brown, tan, red and grey (GP)	230-240'	2 ft/min
	- Gravel becomes coarser to 265 and sand diminishes	240-250'	1.4 ft/min
	- Gravel changes to fine (granular) gravel at 265' with coarse to very coarse sand	250-260'	1.1 ft/min
276	BASALT or ANDESITE; dark brown, medium hard, closely spaced fractures	260-270'	1.1 ft/min
280	Bottom of Hole	270-280'	.8 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-2

LEGAL LOCATION: T9S R14E S1 TRACTNE 1/4 NE 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 3-19-91 DATE COMPLETED: 3-25-91 DRILLING COMPANY/DRILLER: Walker Water Systems/F. Walker LOGGED BY: P. Spillers

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water & Quick Foam

TOTAL DEPTH DRILLED (ft): 400 TOTAL DEPTH CASED (ft): 255 INTERVAL PERFORATED from: 229.9 to: 249.3 DIAMETER OF CASING: 4" PVC TYPE OF CASING: _____

METHOD OF PERFORATION: _____ Open Hole DURING WELL CONSTRUCTION WAS/WERE: YES NO
 _____ Open Bottom YES NO
 _____ Saw Slotted WELL DEVELOPED X _____
X Factory 0.020 (size) WELL PUMPED _____ X
 _____ OTHER (specify) _____ WATER SAMPLES COLLECTED _____ X
 MATERIAL SAMPLES COLLECTED X _____

ANNULAR COMPLETION CHARACTERISTICS
 WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: Concrete from: 0 to: 6'
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 6' to: 190'
 FILTER PACK: Type: Sand from: 190' to: 400'

STATIC WATER LEVEL FT: 195.57' MEASURING POINT DATE: 3-28-91 DESCRIPTION/ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +0.96'

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0	TOPSOIL, silty SAND; fine grained, sod, organics	0-5'	
0.5	Clayey SAND; medium dense, moist, slightly plastic, fine grained, slightly cemented below 1', brown (SC)	5-10'	1 ft/min
1.5	Silty to Clayey SAND with Gravel; slightly moist, medium dense, slightly to nonplastic, slightly to moderately cemented, some basalt fragments, light brown (SC/SM)	10-15'	1 ft/min
6	BASALT; dark grey, moderately hard, moderately closely jointed, severely weathered	15-20'	1 ft/min
	NOTE: soil filled fractures from 6' to 8' widely fractured below 10', hard void from 31.1' to 31.8' slightly fractured from 51.7' to 57.5' & 61.1' to 67.2' (hole caving between 60' & 70')	20-30'	1 ft/min
		30-40'	0.8 ft/min
		40-50'	0.8 ft/min
67.2	BASALT; brown, soft, severely weathered to decomposed, highly fractured, FeO ₂ stained	50-60'	0.8 ft/min
	circulation loss from 85' to 87', first groundwater	60-70'	2 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO.: 190-1496

PROJECT: Clear Lakes Grade

WELL NO.: MW-2

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
		70-80'	5 ft/min
86.6	BASALT; moderately hard, very closely fractured, severely weathered, grey brown	80-90'	1 ft/min
92	BASALT; orange brown, soft, severely weathered to decomposed, highly fractured	90-100'	3.5 ft/min
		100-105'	1.2 ft/min
105	BASALT; grey brown, moderately hard, moderately weathered	105-110'	0.8 ft/min
	NOTE: gradual change to hard or very hard between 105' to 110'	110-117'	0.5 ft/min
	: open vertical joint or fracture from 117.5 to 123' filled with very soft, pale yellow to green claystone	117-120'	0.2 ft/min
124	BASALT; grey, hard, moderately weathered	120-130'	0.3 ft/min
133.3	BASALT; soft to moderately hard, brown, severely weathered	130-140'	1 ft/min
138	BASALT; black, hard, closely fractured, vesicular, slightly to moderately weathered	140-150'	1 ft/min
		150-160'	0.8 ft/min
		160-170'	0.7 ft/min
178	BASALT; brown to black, moderately hard, closely fractured, moderately weathered	170-180'	0.7 ft/min
185	Silty GRAVEL with Sand; saturated, nonplastic, subangular to rounded, fine grained, brown (GM/GP)	180-185'	1 ft/min
	NOTE: increase in groundwater below 185'	185-190'	5 ft/min
		190-200'	3 ft/min
		200-210'	3 ft/min
		210-220'	3 ft/min
		220-230'	5 ft/min
		230-240'	3 ft/min
245	Silty SAND with GRAVEL; saturated, nonplastic, subrounded to rounded, gravel is fine grained, brown (SM/SP)	240-250'	3 ft/min
		250-260'	3 ft/min
263	SANDSTONE; brown, moderately hard, fine to coarse grained, subangular to rounded	260-270'	1 ft/min
	NOTE: strong basalt component in sandstone between 272' & 297', fine sand and drilling fluids are black	270-280'	0.8 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-3S

LEGAL LOCATION: T9S R15E S6 TRACTNW 1/4 NW 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 4-2-91 DATE COMPLETED: 4-3-91 DRILLING COMPANY/DRILLER: Walker Water System/F. Walker LOGGED BY: P. Spillers

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water & Quick Foam

TOTAL DEPTH DRILLED (ft): 115 TOTAL DEPTH CASED (ft): 114.3 INTERVAL PERFORATED from: 89.2 DIAMETER OF CASING: 4" PVC
 OR SCREENED (ft): to: 108.6 TYPE OF CASING: _____

METHOD OF PERFORATION: _____ Open Hole
 _____ Open Bottom
 _____ Saw Slotted
 Factory 0.02" (size)
 _____ OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE:
 YES NO
 WELL DEVELOPED _____
 WELL PUMPED _____
 WATER SAMPLES COLLECTED _____
 MATERIAL SAMPLES COLLECTED _____

ANNULAR COMPLETION CHARACTERISTICS
 WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: concrete from: 0 to: 5
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 5 to: 75
 FILTER PACK: Type: Sand from: 75 to: 115

STATIC WATER LEVEL FT: 90.4' MEASURING POINT DATE: 4-3-91 DESCRIPTION/ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +0.93

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0	TOPSOIL, Silty CLAY; sod, organics	0-10'	0.7 ft/min
0.5	Silty SAND; moist, medium dense, slightly plastic, fine grained, light brown, (SM)	10-20'	0.8 ft/min
1.7	BASALT; dark grey, moderately hard, moderately closely jointed or fractured, moderately weathered, vesicular	20-30'	1 ft/min
	NOTE: closely fractured between 19.5' & 25'	30-40'	1 ft/min
	NOTE: moderately hard to hard between 40 & 62.5', vesicles decrease	40-50'	0.5 ft/min
62.5	BASALT; dark grey to brown, moderately hard, moderately closely fractured, moderately to severely weathered	50-60'	0.8 ft/min
	NOTE: predominately dark grey below 72.4', closely fractured	60-70'	0.8 ft/min
	: occasional light brown clay in fractures below 85', first groundwater	70-80'	0.9 ft/min
		80-90'	0.8 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-3D

LEGAL LOCATION: T9S R15E S6 TRACTNW 1/4 NW 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 4-3-91 DATE COMPLETED: 4-4-91 DRILLING COMPANY/DRILLER: Walker Water System/F. Walker LOGGED BY: P. Spillers

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water & Quick Foam

TOTAL DEPTH DRILLED (ft): 220 TOTAL DEPTH CASSED (ft): 218 INTERVAL PERFORATED from: 192.9 DIAMETER OF CASING: 4" PVC
 OR SCREENED (ft): to: 212.3 TYPE OF CASING: _____

METHOD OF PERFORATION: Open Hole Open Bottom Saw Slotted Factory 0.02" (size) OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE:

	YES	NO
WELL DEVELOPED	_____	<input checked="" type="checkbox"/>
WELL PUMPED	_____	<input checked="" type="checkbox"/>
WATER SAMPLES COLLECTED	_____	<input checked="" type="checkbox"/>
MATERIAL SAMPLES COLLECTED	<input checked="" type="checkbox"/>	_____

ANNULAR COMPLETION CHARACTERISTICS

WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: concrete from: 0 to: 6'
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 6' to: 173'
 FILTER PACK: Type: Sand from: 173' to: 218'

STATIC WATER LEVEL FT: 89.0' MEASURING POINT DATE: 4-4-91 DESCRIPTION/ ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +0.96

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0	Silty SAND; slightly moist, dense, nonplastic, trace of fine gravel, light brown (SM)	0-10'	0.6 ft/min
2	BASALT; dark grey, moderately hard, moderately closely fractured, moderately to severely weathered	10-20'	0.8 ft/min
	NOTE: soil fills fractures to 15', moderately hard below 15'	20-30'	0.8 ft/min
	: fractured zone at 7.9' to 8.2'	30-40'	0.8 ft/min
	: closely fractured, soft between 20.8' & 23.7'	40-50'	0.5 ft/min
	: moderately hard to hard between 40' & 50.4'	50-60'	0.8 ft/min
	: soft below 87'	60-70'	0.9 ft/min
		70-80'	0.9 ft/min
91.6	BASALT; brown to dark grey, very soft, very closely fractured, severely weathered (soil-like) to decomposed NOTE: numerous clay fragments in cuttings, first groundwater	80-90'	1 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-4S

LEGAL LOCATION: T9S R14E S1 TRACTNE 1/4 NE 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 3-27-91 DATE COMPLETED: 4-1-91 DRILLING COMPANY/DRILLER: Walker Water System/F. Walker LOGGED BY: P. Spillers

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water & Quick Foam

TOTAL DEPTH DRILLED (ft): 110 TOTAL DEPTH CASED (ft): 110 INTERVAL PERFORATED OR SCREENED (ft): from: 84.6 to: 104.3 DIAMETER OF CASING: 4" PVC TYPE OF CASING: _____

METHOD OF PERFORATION: _____ Open Hole
 _____ Open Bottom
 _____ Saw Slotted
 Factory 0.02" (size)
 _____ OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE:

WELL DEVELOPED	YES	NO
WELL PUMPED	<u>X</u>	_____
WATER SAMPLES COLLECTED	_____	<u>X</u>
MATERIAL SAMPLES COLLECTED	<u>X</u>	_____

ANNULAR COMPLETION CHARACTERISTICS
 WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: concrete from: 0 to: 7'
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 7' to: 73'
 FILTER PACK: Type: Sand from: 73' to: 110'

STATIC WATER LEVEL FT: 81.6' MEASURING POINT DATE: 4-1-91 DESCRIPTION/ ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +1.29

REMARKS: _____

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	DRILLING RATE	
		Interval	Rate (ft/min)
0	TOPSOIL, Silty SAND; sod, organics	0-5'	.7 ft/min
1	Silty SAND; moist, medium dense, fine grained, slightly plastic, light brown (SM)	5-10'	.8 ft/min
2.6	BASALT; dark grey, soft, moderately closely fractured, moderately weathered, vesicular	10-15'	.6 ft/min
	NOTE: clayey cuttings, brown clay fills some fractures to 20'	15-20'	.7 ft/min
	: fracture zone at 22.2'	20-30'	.7 ft/min
22.2	BASALT; dark grey, hard, moderately closely fractured, moderately weathered, vesicular	30-40'	1.2 ft/min
	NOTE: some closely spaced, open fractures between 36.1' & 38', loss of circulation between 38' & 90'	40-50'	1 ft/min
57.1	BASALT; brown, very closely fractured, severely weathered with clay filling, soft	50-60'	1.2 ft/min
		60-70'	5 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO: 190-1496
 PROJECT: Clear Lakes Grade STATE: ID COUNTY: Gooding WELL NO.: MW-4D

LEGAL LOCATION: T9S R14E S1 TRACTNE 1/4 NE 1/4 DESCRIPTIVE LOCATION: See Text

DATE STARTED: 3-29-91 DATE COMPLETED: 4-2-91 DRILLING COMPANY/DRILLER: Walker Water System/F. Walker LOGGED BY: P. Spillers

DRILLING METHOD: Air Rotary BOREHOLE DIAMETER (In): 8" DRILL FLUIDS USED: Water & Quick Foam

TOTAL DEPTH DRILLED (ft): 250 TOTAL DEPTH CASED (ft): 207.5 INTERVAL PERFORATED from: 182.4 DIAMETER OF CASING: 4" PVC
 OR SCREENED (ft): to: 201.8 TYPE OF CASING: _____

METHOD OF PERFORATION: Open Hole Open Bottom Saw Slotted Factory 0.02" (size) OTHER (specify) _____

DURING WELL CONSTRUCTION WAS/WERE:

	YES	NO
WELL DEVELOPED	<input checked="" type="checkbox"/>	<input type="checkbox"/>
WELL PUMPED	<input type="checkbox"/>	<input checked="" type="checkbox"/>
WATER SAMPLES COLLECTED	<input type="checkbox"/>	<input checked="" type="checkbox"/>
MATERIAL SAMPLES COLLECTED	<input checked="" type="checkbox"/>	<input type="checkbox"/>

ANNULAR COMPLETION CHARACTERISTICS
 WELL PROTECTOR: Length 36" Diam. 6" SURFACE SEAL: Type: concrete from: 0 to: 5'
 LOCK NO.: Dolphin BACKFILL: Material: Bentonite from: 5' to: 168'
 FILTER PACK: Type: Sand from: 168' to: 207.5'

STATIC WATER LEVEL FT: 179.5 MEASURING POINT DATE: 4-1-91 DESCRIPTION/ ELEVATION FT: top of PVC MEASURING POINT RELATIVE TO GROUND SURFACE (+/-): +0.97

REMARKS: _____

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
0 - 0.5	TOPSOIL, sod, organics, Silty SAND	0-2.4	
0.5	Silty to Clayey SAND; moist, slightly plastic, fine grained, some fine gravel, tan (SC/SM)	2.4-5.0'	0.5 ft/min
2.4	BASALT; dark grey to black, moderately hard to soft, moderately closely fractured, moderately weathered, vesicular	5-10'	0.6 ft/min
	NOTE: clay filled fractures to 15'	10-15'	0.3 ft/min
	: hard between 40' & 46.4'	15-20'	0.3 ft/min
	: highly fractured at 60.2	20-30'	0.5 ft/min
		30-40'	0.4 ft/min
		40-50'	0.3 ft/min
		50-60'	0.4 ft/min

MONITORING WELL LITHOLOGIC AND COMPLETION LOG

JOB NO.: 190-1496
 PROJECT: Clear Lakes Grade

WELL NO.: MW-4D

DRILLING RATE

INTERVAL (FT) below ground surface	LITHOLOGIC DESCRIPTION	Interval	Rate (ft/min)
64	BASALT; dark brown, moderately hard, very closely fractured-filled with claystone, severely weathered, vesicular	60-70'	1.5 ft/min
		70-80'	2.2 ft/min
83.4	BASALT; brown, severely weathered, soft, very closely fractured	80-90'	1.8 ft/min
	NOTE: open fracture from 99.5' to 100', first groundwater at 90'	90-100'	5.3 ft/min
108.3	BASALT; dark grey, moderately hard, moderately fractured, moderately weathered	100-110'	2 ft/min
	NOTE: contains groundwater	110-120'	0.9 ft/min
	NOTE: hard below 130', some claystone filled fractures	120-130'	0.7 ft/min
	: closely fractured or jointed below 133'	130-140'	0.4 ft/min
		140-150'	0.4 ft/min
		150-160'	0.5 ft/min
	: clay lens at 173', low to medium PI, dark grey	160-170'	0.5 ft/min
		170-180'	0.6 ft/min
181	Poorly Graded GRAVEL with Sand; dense, saturated, nonplastic, predominately fine grained, subrounded, brown to black (GP/GM)	180-190'	2.2 ft/min
		190-200'	4.2 ft/min
195	Poorly Graded SAND with Gravel; dense, saturated, nonplastic, predominately well graded, subrounded, brown (SP/SM)	200-210'	5 ft/min
		210-220'	4.3 ft/min
		220-230'	4.6 ft/min
		230-240'	3.3 ft/min
250	Bottom of Hole	240-250'	3.5 ft/min

APPENDIX B

**Analytical Reports and Chain-of-Custody Forms
Water Sampling Procedures**

Prior to sampling, wells were developed using a mechanical bailer until the water was relatively clear or at least three bore volumes. Samples were then obtained using a stainless steel bailer. Water samples from springs were collected directly from the stream near the point of discharge of measurement stations.

Pre-cleaned 500 milliliter (ml) bottles with tight fitting lids were filled for laboratory analysis of cation/anion balance. Samples were kept cool with ice packs following collection and during shipment to the laboratory. Samples were also analyzed in the field for temperature, pH, and specific conductance.

All samples remained in the custody of Chen-Northern field personnel until shipment to the laboratory. Time and date of sample collection, sample identification numbers, custody personnel, and time and date received by the lab were transcribed on the chain-of-custody forms for each sample. All sample containers were transferred directly to the laboratory by overnight courier.

A member of the **HIH** group of companies

600 SOUTH 25TH STREET
P. O. BOX 30815
BILLINGS, MT 59107
(406) 248-9161
FAX (406) 248-9282

TECHNICAL REPORT



REPORT TO:

ATTN: MR. PAUL SPILLERS
CHEN-NORTHERN, INC.
P. O. BOX 7777
BOISE, ID 83707

DATE: May 6, 1991
JOB NUMBER: 87-933
SHEET: 1 OF 15
INVOICE NO.: 113849

REPORT OF: Water Analysis - Clear Lake Grade (190-1496)

Sample Identification:

On April 16, 1991, these water samples (Lab Nos. 114392 - 114405) were received in our laboratory for analysis. Tests were conducted in accordance with the U.S. Environmental Protection Agency Manual EPA 600/4-79-020, "Methods for Chemical Analysis of Water and Wastes." The results of the analysis are shown on the following pages.

A < sign indicates less than the reported value was present in the sample.

Reviewed by

ba

Client Name: CHEN-NORTHERN, INC. BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 2 of 15

Laboratory No.: 114392
 Sample Name: MW-1S
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 14:50:00

PARAMETER	AVERAGE VALUE	DATE ANALYZED
Anions:		
Chloride as Cl <i>35.45</i>	29 mg/l	04/25/91
Fluoride as F <i>14.00</i>	0.93 mg/l	04/24/91
Sulfate as SO4 <i>48.10</i>	41 mg/l	04/23/91
Total Alkalinity as CaCO3 <i>50.00</i>	258 mg/l	04/17/91
Cations:		
Calcium as Ca <i>20.04</i>	51 mg/l	04/17/91
Magnesium as Mg <i>12.15</i>	22 mg/l	04/17/91
Potassium as K <i>34.1</i>	6.6 mg/l	04/25/91
Sodium as Na <i>22.99</i>	46 mg/l	04/17/91
Nutrients:		
Nitrate + Nitrite as N <i>14.00</i>	0.99 mg/l	04/19/91

1015 - 105

Client Name: CHEN-NORTHERN, INC. BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (87-933)

May 6, 1991
 Sheet 3 of 15

Laboratory No.: 114393
 Sample Name: MW-1D
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 15:15:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	42	mg/l	04/25/91
Fluoride as F	0.49	mg/l	04/24/91
Sulfate as SO ₄	53	mg/l	04/23/91
Total Alkalinity as CaCO ₃	154	mg/l	04/17/91
Cations:			
Calcium as Ca	47	mg/l	04/17/91
Magnesium as Mg	17	mg/l	04/17/91
Potassium as K	7.5	mg/l	04/25/91
Sodium as Na	27	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.47	mg/l	04/19/91

Handwritten notes:
 5/10/91
 1155

Client Name: CHEN-NORTHERN, INC. BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 4 of 15

Laboratory No.: 114394
 Sample Name: MW-2
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 17:30:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	55	mg/l	04/25/91
Fluoride as F	0.58	mg/l	04/24/91
Sulfate as SO ₄	67	mg/l	04/23/91
Total Alkalinity as CaCO ₃	186	mg/l	04/18/91
Cations:			
Calcium as Ca	24	mg/l	04/17/91
Magnesium as Mg	10	mg/l	04/17/91
Potassium as K	5.2	mg/l	04/25/91
Sodium as Na	108	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.71	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC. BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 5 of 15

Laboratory No.: 114395
 Sample Name: MW-3S
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 18:35:00

PARAMETER	AVERAGE VALUE	DATE ANALYZED
Anions:		
Chloride as Cl	40 mg/l	04/25/91
Fluoride as F	0.55 mg/l	04/24/91
Sulfate as SO4	44 mg/l	04/19/91
Total Alkalinity as CaCO3	198 mg/l	04/18/91
Cations:		
Calcium as Ca	51 mg/l	04/17/91
Magnesium as Mg	24 mg/l	04/17/91
Potassium as K	6.7 mg/l	04/25/91
Sodium as Na	35 mg/l	04/17/91
Nutrients:		
Nitrate + Nitrite as N	2.86 mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 6 of 15

Laboratory No.: 114396
 Sample Name: MW-3D
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 19:05:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	40	mg/l	04/25/91
Fluoride as F	0.55	mg/l	04/24/91
Sulfate as SO4	269 49	mg/l	04/23/91
Total Alkalinity as CaCO3	179	mg/l	04/18/91
Cations:			
Calcium as Ca	56	mg/l	04/17/91
Magnesium as Mg	22	mg/l	04/17/91
Potassium as K	13.5 6.5	mg/l	04/25/91
Sodium as Na	29	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	2.24	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC. BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 7 of 15

Laboratory No.: 114397
 Sample Name: MW-4S
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 17:50:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	27	mg/l	04/25/91
Fluoride as F	0.53	mg/l	04/24/91
Sulfate as SO4	57	mg/l	04/23/91
Total Alkalinity as CaCO3	330.246	mg/l	04/18/91
Cations:			
Calcium as Ca	60	mg/l	04/17/91
Magnesium as Mg	23	mg/l	04/17/91
Potassium as K	6.3	mg/l	04/25/91
Sodium as Na	46	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	0.94	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 8 of 15

Laboratory No.: 114398
 Sample Name: MW-4D
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 16:00:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	38	mg/l	04/25/91
Fluoride as F	0.53	mg/l	04/24/91
Sulfate as SO4	40	mg/l	04/23/91
Total Alkalinity as CaCO3	159	mg/l	04/18/91
Cations:			
Calcium as Ca	45	mg/l	04/17/91
Magnesium as Mg	16	mg/l	04/17/91
Potassium as K	7.3	mg/l	04/25/91
Sodium as Na	33	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.79	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
Project No.: 87-933
Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
Sheet 9 of 15

Laboratory No.: 114399
Sample Name: 1W
Sample Date: 04/12/91
Collected by: Christopher Kaetzel
Time Sampled: 20:25:00

PARAMETER	AVERAGE VALUE	DATE ANALYZED
Anions:		
Chloride as Cl	38 mg/l	04/25/91
Fluoride as F	0.53 mg/l	04/24/91
Sulfate as SO ₄	225 25 mg/l	04/23/91
Total Alkalinity as CaCO ₃	161 mg/l	04/18/91
Cations:		
Calcium as Ca	45 mg/l	04/17/91
Magnesium as Mg	19 mg/l	04/17/91
Potassium as K	63.3 4.3 mg/l	04/25/91
Sodium as Na	25 mg/l	04/17/91
Nutrients:		
Nitrate + Nitrite as N	1.44 mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 10 of 15

Laboratory No.: 114400
 Sample Name: 2W UPPER
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 20:20:00

PARAMETER	AVERAGE VALUE	DATE ANALYZED
Anions:		
Chloride as Cl	36 mg/l	04/25/91
Fluoride as F	0.78 mg/l	04/24/91
Sulfate as SO4	37 mg/l	04/23/91
Total Alkalinity as CaCO3	213 mg/l	04/18/91
Cations:		
Calcium as Ca	47 mg/l	04/17/91
Magnesium as Mg	26 mg/l	04/17/91
Potassium as K	4.6 mg/l	04/25/91
Sodium as Na	33 mg/l	04/17/91
Nutrients:		
Nitrate + Nitrite as N	1.17 mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 11 of 15

Laboratory No.: 114401
 Sample Name: 3W
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 20:20:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	40	mg/l	04/25/91
Fluoride as F	0.53	mg/l	04/24/91
Sulfate as SO4	245 40	mg/l	04/23/91
Total Alkalinity as CaCO3	164	mg/l	04/18/91
Cations:			
Calcium as Ca	45	mg/l	04/17/91
Magnesium as Mg	19	mg/l	04/17/91
Potassium as K	4.6	mg/l	04/25/91
Sodium as Na	25	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.41	mg/l	04/19/91

1.41 CA

Client Name: CHEN-NORTHERN, INC., BOISE, ID
Project No.: 87-933
Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
Sheet 12 of 15

Laboratory No.: 114402
Sample Name: 4W
Sample Date: 04/12/91
Collected by: Christopher Kaetzel
Time Sampled: 20:10:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	40	mg/l	04/25/91
Fluoride as F	0.53	mg/l	04/24/91
Sulfate as SO4	249 47	mg/l	04/23/91
Total Alkalinity as CaCO3	161	mg/l	04/18/91
Cations:			
Calcium as Ca	54	mg/l	04/17/91
Magnesium as Mg	107 21	mg/l	04/17/91
Potassium as K	4.4	mg/l	04/25/91
Sodium as Na	30	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.37	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 13 of 15

Laboratory No.: 114403
 Sample Name: 5W
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 20:00:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	39	mg/l	04/25/91
Fluoride as F	0.58	mg/l	04/24/91
Sulfate as SO4	263 52	mg/l	04/23/91
Total Alkalinity as CaCO3	171	mg/l	04/18/91
Cations:			
Calcium as Ca	55	mg/l	04/17/91
Magnesium as Mg	21	mg/l	04/17/91
Potassium as K	4.3	mg/l	04/25/91
Sodium as Na	30	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.30	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
 Project No.: 87-933
 Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
 Sheet 14, Of 15

Laboratory No.: 114404
 Sample Name: 6W
 Sample Date: 04/12/91
 Collected by: Christopher Kaetzel
 Time Sampled: 20:00:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	37	mg/l	04/25/91
Fluoride as F	0.55	mg/l	04/24/91
Sulfate as SO ₄	52	mg/l	04/23/91
Total Alkalinity as CaCO ₃	159	mg/l	04/18/91
Cations:			
Calcium as Ca	53	mg/l	04/17/91
Magnesium as Mg	21	mg/l	04/17/91
Potassium as K	4.3	mg/l	04/25/91
Sodium as Na	29	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.31	mg/l	04/19/91

Client Name: CHEN-NORTHERN, INC., BOISE, ID
Project No.: 87-933
Project Name: Water Analysis - Clear Lake Grade (190-1496)

May 6, 1991
Sheet 15 of 15

Laboratory No.: 114405
Sample Name: 7W
Sample Date: 04/12/91
Collected by: Christopher Kaetzel
Time Sampled: 20:00:00

PARAMETER	AVERAGE VALUE		DATE ANALYZED
Anions:			
Chloride as Cl	38	mg/l	04/25/91
Fluoride as F	0.58	mg/l	04/24/91
Total Alkalinity as CaCO ₃	251 166	mg/l	04/18/91
Sulfate as SO ₄	46	mg/l	04/23/91
Cations:			
Calcium as Ca	53	mg/l	04/17/91
Magnesium as Mg	21	mg/l	04/17/91
Potassium as K	4.4	mg/l	04/25/91
Sodium as Na	29	mg/l	04/17/91
Nutrients:			
Nitrate + Nitrite as N	1.30	mg/l	04/19/91

<input type="checkbox"/> BILLINGS 600 SOUTH 25TH STREET P. O. BOX 30616 BILLINGS, MT 59107 (406) 245-9181 FAX (406) 248-9282		<input type="checkbox"/> CASPER 606 N. WAREHOUSE ROAD P. O. BOX 2699 CASPER, WY 82502 (307) 294-2138 FAX (307) 296-8148		<input type="checkbox"/> GREAT FALLS 828 SMELTER AVENUE P. O. BOX 981 GREAT FALLS, MT 59408 (406) 453-1841 FAX (406) 787-8070		<input type="checkbox"/> HELENA 1810 B STREET P. O. BOX 4899 HELENA, MT 59605 (406) 445-0210 FAX (406) 448-0759		<input type="checkbox"/> TRI-CITIES 2214 NORTH 4TH AVENUE P. O. BOX 3601 TRI-CITIES, WA 99002 (509) 847-1071 FAX (509) 847-1073	
Proj. No. 190-1491a	Project Name Clena Lakes Grade	Station Location	No. of Containers	Remarks	Relinquished by: (Signature)	Date / Time	Rec'd by: (Signature)	Date / Time	
Samplers: (Signature) C. Kautz	Paul Appellus								
Sta. No.	Date	Time							
MW-15	4-12-91	14 50	1						
MW-1P		15 15	1						
MW-2		17 30	1						
MW-3S		18 35	1						
MW-3D		19 05	1						
MW-4S		17 50	1						
MW-4D		16 00	1						
DW-B		19 20	1						
DW-A		19 30	1						
DW-C		19 45	1						
1W		20 25	1						
2W Upper		20 30	1						
3W		20 20	1						
4W		20 10	1						
5W		20 00	1						
6W		20 00	1						
Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	
(Signature)	4/15/91	(Signature)	4/15/91	(Signature)	4/16/91	(Signature)	4/16/91	(Signature)	
Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	
Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	Date / Time	Relinquished by: (Signature)	

APPENDIX C

Area Well Drillers Reports

USE TYPEWRITER OR BALL POINT PEN

State of Idaho Department of Water Resources

WELL DRILLER'S REPORT

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

1. WELL OWNER

Name John Madolemic

Address Wilson Hill Idaho

Owner's Permit No. _____

7. WATER LEVEL

Static water level 70 feet below land surface

Flowing? Yes No G.P.M. flow _____

Temperature _____ ° F. Quality _____

Artesian closed-in pressure _____ p.s.i.

Controlled by Valve Cap Plug

2. NATURE OF WORK

New well Deepened Replacement

Abandoned (describe method of abandoning) _____

8. WELL TEST DATA

Pump Baller Other

Discharge G.P.M.	Draw Down	Hours Pumped
<u>no test</u>		

3. PROPOSED USE

Domestic Irrigation Test Other (specify type) _____

Municipal Industrial Stock Waste Disposal or Injection

9. LITHOLOGIC LOG

Hole Diam.	Depth		Material	Water	
	From	To		Yes	No
<u>16</u>	<u>0</u>	<u>11</u>	<u>top soil</u>		
	<u>4</u>	<u>25</u>	<u>gray loam</u>		
	<u>23</u>	<u>35</u>	<u>red loam</u>		
	<u>55</u>	<u>57</u>	<u>gray loam</u>		
	<u>70</u>	<u>83</u>	<u>hard loam under</u>		

4. METHOD DRILLED

Cable Rotary Dug Other

5. WELL CONSTRUCTION

Diameter of hole 16 inches Total depth 83 feet

Casing schedule: Steel Concrete

Thickness	Diameter	From	To
<u>260</u> inches	<u>16</u> inches	<u>1</u> feet	<u>10</u> feet
_____ inches	_____ inches	_____ feet	_____ feet
_____ inches	_____ inches	_____ feet	_____ feet
_____ inches	_____ inches	_____ feet	_____ feet
_____ inches	_____ inches	_____ feet	_____ feet

Was casing drive shoe used? Yes No

Was a packer or seal used? Yes No

Perforated? Yes No

How perforated? Factory Knife Torch

Size of perforation _____ inches by _____ inches

Number	From	To
_____ perforations	_____ feet	_____ feet
_____ perforations	_____ feet	_____ feet
_____ perforations	_____ feet	_____ feet

Well screen installed? Yes No

Manufacturer's name _____

Type _____ Model No. _____

Diameter _____ Slot size _____ Set from _____ feet to _____ feet

Diameter _____ Slot size _____ Set from _____ feet to _____ feet

Gravel packed? Yes No Size of gravel _____

Placed from _____ feet to _____ feet

Surface seal depth 19 Material used in seal Cement grout

Padding clay Well settings

Sealing procedure used Shurry fill Temporary surface casing

Overbars to seal depth

6. LOCATION OF WELL

Sketch map location must agree with written location.

Subdivision Name _____

Lot No. _____ Block No. _____

County Blaine

3W 4SE X Sec 36 T. 9 N. R. 14 E

10. Work started _____ finished March 2-1962

11. DRILLER'S CERTIFICATION

Firm Name John Madolemic

Address Wilson Hill Idaho Date Apr 11

Signed by (Firm Official) James Madolemic

Operator Russ Harley

USE ADDITIONAL SHEETS IF NECESSARY. FORWARD THE WHITE COPY TO THE DEPARTMENT.

REPORT OF WELL DRILLER
State of Idaho

State law requires that this report shall be filed with the State Reclamation Engineer within 30 days after completion or abandonment of the well.

WELL OWNER:
Name Blick
Address WENDELL

Owner's Permit No. _____
NATURE OF WORK (check): Replacement well
New well Deepened Abandoned
Water is to be used for: irrigation
METHOD OF CONSTRUCTION: Rotary Cable
Dug Other _____

(explain)
CASING SCHEDULE: Threaded _____ Welded 7
"Diam. from _____ ft. to _____ ft.
Thickness of casing: _____ Material: _____
Steel concrete wood other

(explain)
PERFORATED? Yes No Type of perforator used: _____

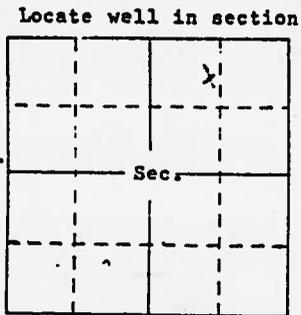
Size of perforations: _____ " by _____ "
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.

WAS SCREEN INSTALLED? Yes No
Manufacturer's name _____
Type _____ Model No. _____
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.

CONSTRUCTION: Well gravel packed? Yes
No size of gravel _____ Gravel placed from _____ ft. to _____ ft. Surface seal provided? Yes No To what depth? _____ ft. Material used in seal: _____

Did any strata contain unusable water? Yes
No Type of water: _____
Depth of strata _____ ft. Method of sealing strata off: _____

Surface casing used? Yes No
Cemented in place? Yes No



LOCATION OF WELL: County _____
Blk NE Sec. 36 T. 8 S R. 14 E X

Size of drilled hole: _____ Total depth of well: _____ Standing water level below ground: _____ Temp. Fahr. _____ Test delivery: _____ gpm or _____ cfs Pump? Bail
Size of pump and motor used to make test: _____

Length of time of test: _____ Hrs. _____ Min.
Drawdown: _____ ft. Artesian pressure: ft. above land surface _____ Give flow _____ cfs or _____ gpm. Shutoff pressure: _____
Controlled by: Valve Cap Plug
No control Does well leak around casing? Yes No

DEPTH		MATERIAL	WATER
FROM	TO		YES OR NO
FEET	FEET		
0	31	Tap, soil	
3	32	Clay	
32	58	10-lobed, blue	
58	76	Clay, blue, sand	
76	92	Clay, blue	
92	97	12-lobed, blue, sand	
		rest of water	
		water stand at 68 ft	
		3 1/2 water at 68 ft	
		70 ft 72 casing	
		15 ft perforations	
		16" hole to 70 ft	
		12" hole from 70 ft to 92 ft	
			1/2 in.

Work started: _____
Work finished: _____
Well Driller's Statement: This well was drilled under my supervision and this report is true to the best of my knowledge.
Name: LIBERTY

Address: WENDELL, IDA
Signed by: Carl Thullen
License No. 20 Date: 5-25-70

USE BALL POINT PEN

WELL DRILLER'S REPORT

State law requires that this report be filed with the Director, Department of Water Resources within _____ days after the completion or abandonment of the well. _____ Department of Water Resources

Eastern District Office

1. WELL OWNER

Name North Side Canal Company

Address Jerome, Idaho

Owner's Permit No. _____

7. WATER LEVEL

Static water level 62 feet below land surface

Flowing? Yes No G.P.M. flow _____

Temperature _____ ° F, Quality _____

Artesian closed-in pressure _____ p.s.i.

Controlled by Valve Cap Plug

2. NATURE OF WORK

New well Deepened Replacement

Abandoned (Describe method of abandoning) _____

8. WELL TEST DATA NONE

Pump Bailor Other

Discharge G.P.M.	Draw Down	Hours Pumped

3. PROPOSED USE

Domestic Irrigation Test Other (specify type) _____

Municipal Industrial Stock Waste Disposal or Injection

9. LITHOLOGIC LOG

Hole Diam.	Depth		Material	Water	
	From	To		Yes	No
8	0	1	Top Soil		X
	1	4	Broken Gray Basalt		
	4	12	Hard Gray Basalt		
	12	16	Med Hard Brown Basalt		
8/6	16	32	Hard Gray Basalt		
6	32	41	Hard Gray Basalt w/small breaks		
	41	43	Very Hard Gray Basalt		
	43	45	Med Hard Gray Basalt w/sm. breaks		
	45	49	Hard Gray Basalt		
	49	60	Hard Gray Basalt w/small breaks	X	
	60	65	Hard Gray Basalt /large breaks	X	
	65	80	Med Hard Grayish Brown Basalt	X	
	80	89	Hard Gray Basalt		X
	89	95	Hard Gray Basalt /sm. breaks	X	
	95	98	Hard Gray Basalt/lg. breaks	X	

4. METHOD DRILLED

Cable Rotary Dug Other

5. WELL CONSTRUCTION

Diameter of hole 6 inches Total depth 98 feet

Casing schedule: Steel Concrete

Thickness	Diameter	From	To
<u>2.50</u> inches	<u>6.5/BOD</u> inches	<u>1</u> feet	<u>-19'8"</u> feet

Was casing drive shoe used? Yes No

Was a packer or seal used? Yes No

Perforated? Yes No

How perforated? Factory Knife Torch

Size of perforation _____ inches by _____ inches

Number	From	To

Well screen installed? Yes No

Manufacturer's name _____

Type _____ Model No. _____

Diameter _____ Slot size _____ Set from _____ feet to _____ feet

Diameter _____ Slot size _____ Set from _____ feet to _____ feet

Gravel packed? Yes No Size of gravel _____

Placed from _____ feet to _____ feet

Surface seal depth 18 Material used in seal Cement grout

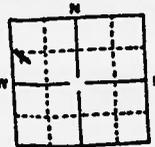
Puddling clay Well cuttings

Sealing procedure used Sherry pit Temporary surface casing

Overbore to seal depth

6. LOCATION OF WELL

Sketch map location must agree with written location.



Subdivision Name _____

Lot No. 2 Block No. _____

County _____ Gooding

SW X NW X Sec. 31 T. 8S N/S. R. 15E BM E/W

10. Work started 10/8/76 finished 10/9/76

11. DRILLER'S CERTIFICATION

SMITH DRILLING & PUMP CO., INC. Firm No. 11

Address 328 W 1st Avenue A Dep. 10/11/76

Signed by (Firm Official) _____ and _____ (Operator)

USE ADDITIONAL SHEETS IF NECESSARY FORWARD THE WHITE COPY TO THE DEPARTMENT

FUJI MICRO SAFETY

STATE OF IDAHO
DEPARTMENT OF WATER RESOURCES
WELL DRILLER'S REPORT

USE TYPEWRITER OR
BALLPOINT PEN

State law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

<p>1. WELL OWNER <i>Phil Black</i></p> <p>Name <i>North Side Farms</i></p> <p>Address <i>P.O. Box 635 Eastford Id.</i></p> <p>Owner's Permit No. <i>36-89-5-029</i></p>	<p>7. WATER LEVEL</p> <p>Static water level <i>76'</i> feet below land surface.</p> <p>Flowing? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No G.P.M. flow _____</p> <p>Artesian closed-in pressure _____ p.s.i.</p> <p>Controlled by: <input type="checkbox"/> Valve <input type="checkbox"/> Cap <input type="checkbox"/> Plug</p> <p>Temperature _____ of Quality _____</p> <p><i>Draw the artesian or temperature zones below</i></p>																																															
<p>2. NATURE OF WORK</p> <p><input checked="" type="checkbox"/> New well <input type="checkbox"/> Deepened <input type="checkbox"/> Replacement</p> <p><input type="checkbox"/> Abandoned (describe abandonment procedures such as materials, plug depths, etc. in lithologic log)</p>	<p>8. WELL TEST DATA</p> <p><input type="checkbox"/> Pump <input checked="" type="checkbox"/> Bailor <input type="checkbox"/> Air <input type="checkbox"/> Other _____</p> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Discharge G.P.M.</th> <th>Pumping Level</th> <th>Hours Pumped</th> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </table>	Discharge G.P.M.	Pumping Level	Hours Pumped																																												
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<p>3. PROPOSED USE</p> <p><input checked="" type="checkbox"/> Domestic <input type="checkbox"/> Irrigation <input type="checkbox"/> Test <input type="checkbox"/> Municipal</p> <p><input type="checkbox"/> Industrial <input type="checkbox"/> Stock <input type="checkbox"/> Waste Disposal or Injection</p> <p><input type="checkbox"/> Other _____ (specify type)</p>	<p>9. LITHOLOGIC LOG</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">Bore Diam.</th> <th colspan="2">Depth</th> <th rowspan="2">Material</th> <th rowspan="2">Well Yes No</th> </tr> <tr> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td></td> <td>0</td> <td>3</td> <td>Top Soil</td> <td></td> </tr> <tr> <td></td> <td>3</td> <td>5</td> <td>White TALK ELY</td> <td></td> </tr> <tr> <td></td> <td>5</td> <td>32</td> <td>L2V2</td> <td></td> </tr> <tr> <td></td> <td>32</td> <td>37</td> <td>L2V2 Strip 2 Cylinders</td> <td></td> </tr> <tr> <td></td> <td>39</td> <td>45</td> <td>L2V2</td> <td></td> </tr> <tr> <td></td> <td>45</td> <td>60</td> <td>Grey Marble Hard</td> <td></td> </tr> <tr> <td></td> <td>60</td> <td>101</td> <td>L2V2 50 lbs Cylinders</td> <td></td> </tr> <tr> <td></td> <td>101</td> <td>104</td> <td>Cylinders - 3</td> <td></td> </tr> </tbody> </table>	Bore Diam.	Depth		Material	Well Yes No	From	To		0	3	Top Soil			3	5	White TALK ELY			5	32	L2V2			32	37	L2V2 Strip 2 Cylinders			39	45	L2V2			45	60	Grey Marble Hard			60	101	L2V2 50 lbs Cylinders			101	104	Cylinders - 3	
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<p>4. METHOD DRILLED</p> <p><input type="checkbox"/> Rotary <input type="checkbox"/> Air <input type="checkbox"/> Hydraulic <input type="checkbox"/> Reverse rotary</p> <p><input checked="" type="checkbox"/> Cable <input type="checkbox"/> Dug <input type="checkbox"/> Other _____</p>	<p style="text-align: center; font-size: 2em; border: 1px solid black; padding: 5px;">RECEIVED</p> <p style="text-align: center;">JUL 27 1989</p> <p style="text-align: center;">Department of Water Resources Southern Region Office</p> <p style="text-align: center;">JUL 27 1989</p>																																															
<p>5. WELL CONSTRUCTION</p> <p>Casing schedule: <input checked="" type="checkbox"/> Steel <input type="checkbox"/> Concrete <input type="checkbox"/> Other _____</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Thickness</th> <th>Diameter</th> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td><i>250</i> inches</td> <td><i>6"</i> inches</td> <td><i>1</i> feet</td> <td><i>20</i> feet</td> </tr> <tr> <td>_____ inches</td> <td>_____ inches</td> <td>_____ feet</td> <td>_____ feet</td> </tr> <tr> <td>_____ inches</td> <td>_____ inches</td> <td>_____ feet</td> <td>_____ feet</td> </tr> <tr> <td>_____ inches</td> <td>_____ inches</td> <td>_____ feet</td> <td>_____ feet</td> </tr> </tbody> </table> <p>Was casing drive shoe used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Was a packer or seal used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Perforated? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>How perforated? <input type="checkbox"/> Factory <input type="checkbox"/> Knife <input type="checkbox"/> Torch</p> <p>Size of perforation _____ inches by _____ inches</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Number</th> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td>_____ perforations</td> <td>_____ feet</td> <td>_____ feet</td> </tr> <tr> <td>_____ perforations</td> <td>_____ feet</td> <td>_____ feet</td> </tr> <tr> <td>_____ perforations</td> <td>_____ feet</td> <td>_____ feet</td> </tr> </tbody> </table> <p>Well screen installed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Manufacturer's name _____</p> <p>Type _____ Model No. _____</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Diameter</th> <th>Slot size</th> <th>Set from</th> <th>feet to</th> <th>feet</th> </tr> </thead> <tbody> <tr> <td>_____</td> <td>_____</td> <td>_____</td> <td>_____</td> <td>_____</td> </tr> <tr> <td>_____</td> <td>_____</td> <td>_____</td> <td>_____</td> <td>_____</td> </tr> </tbody> </table> <p>Gravel packed? <input type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Size of gravel _____</p> <p>Placed from _____ feet to _____ feet</p> <p>Surface seal depth <i>19'</i> Material used in seal: <input checked="" type="checkbox"/> Cement grout</p> <p><input type="checkbox"/> Bentonite <input type="checkbox"/> Pudding clay <input checked="" type="checkbox"/> Well Casing</p> <p>Sealing procedure used: <input type="checkbox"/> Slurry pit <input checked="" type="checkbox"/> Temp. surface casing</p> <p><input type="checkbox"/> Overbore to seal depth</p> <p>Method of joining casing: <input type="checkbox"/> Threaded <input type="checkbox"/> Welded <input type="checkbox"/> Solvent Weld</p> <p><input type="checkbox"/> Cemented between strata</p> <p>Describe access port <i>Well C.A.P.</i></p>	Thickness	Diameter	From	To	<i>250</i> inches	<i>6"</i> inches	<i>1</i> feet	<i>20</i> feet	_____ inches	_____ inches	_____ feet	_____ feet	_____ inches	_____ inches	_____ feet	_____ feet	_____ inches	_____ inches	_____ feet	_____ feet	Number	From	To	_____ perforations	_____ feet	_____ feet	_____ perforations	_____ feet	_____ feet	_____ perforations	_____ feet	_____ feet	Diameter	Slot size	Set from	feet to	feet	_____	_____	_____	_____	_____	_____	_____	_____	_____	_____	<p>10.</p> <p>Work started <i>3-28-89</i> finished <i>4-1-89</i></p>
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REPORT OF WELL DRILLER
State of Idaho

RECEIVED
APR 1 1968
Department of Reclamation

State law requires that this report shall be filed with the State Reclamation Engineer within 30 days after completion or abandonment of the well.

WELL OWNER:
Name Frank Henslee
Address Hacarman, Idaho

Owner's Permit No. _____
NATURE OF WORK (check): Replacement well
New well Deepened Abandoned

Water is to be used for: Irrigation

METHOD OF CONSTRUCTION: Rotary Cable
Dug Other _____

CASING SCHEDULE: Threaded _____ Welded _____
"Diam. from _____ ft. to _____ ft.
Thickness of casing: _____ Material: _____
Steel concrete wood other

(explain)
PERFORATED? Yes No Type of perforator used: _____

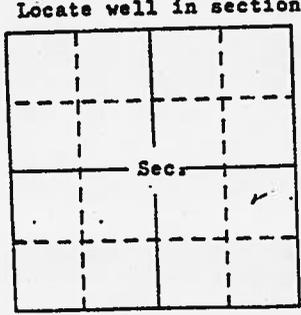
Size of perforations: _____ " by _____ "
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.
perforations from _____ ft. to _____ ft.

WAS SCREEN INSTALLED? Yes No
Manufacturer's name _____
Type _____ Model No. _____
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.

CONSTRUCTION: Well gravel packed? Yes
No size of gravel _____ Gravel placed from _____ ft. to _____ ft. Surface seal provided? Yes No To what depth? _____ ft. Material used in seal: _____

Did any strata contain unusable water? Yes
No Type of water: _____
Depth of strata _____ ft. Method of sealing strata off: _____

Surface casing used? Yes No
Cemented in place? Yes No



LOCATION OF WELL: County Gooding
T. 33 S. R. 14E/W

Size of drilled hole: 1 1/2"
depth of well: 300 ft. Standing water level below ground: 95 ft. Temp. Fahr. _____ Test delivery: _____ gpm or _____ cfs Pump? Bail
Size of pump and motor used to make test: _____

Length of time of test: _____ Hrs. _____ Min.
Drawdown: _____ ft. Artesian pressure: ft. above land surface Give flow _____ cfs or _____ gpm. Shutoff pressure: _____
Controlled by: Valve Cap Plug
No control Does well leak around casing? Yes No

DEPTH	MATERIAL	WATER YES OR NO
FROM TO		
FEET FEET		
155 160	Hard gray lava	
160 217	Black lava, layers of porous lava	
217 228	Hard gray lava	
228 231	Black hard lava	
231 240	Hard gray lava	
240 248	Brown silt	
248 268	Brown sand & gravel, picked up quite a bit of water.	
268 300	Brown sticky clay.	

Work started: Feb. 15, 1968
Work finished: March 1, 1968
Well Driller's Statement: This well was drilled under my supervision and this report is true to the best of my knowledge.
Name: Elmer Austin
Address: Vanston, Idaho
Signed by: Marion Gray Shellen
License No. 573 Date: 3/11/68

Marion Gray Shellen Drilling

Use other side for additional remarks

USGS

STATE OF IDAHO
DEPARTMENT OF WATER RESOURCES
WELL DRILLER'S REPORT

USE TYPEWRITER OR
BALLPOINT PEN

State law requires that this report be filed with the Director, Department of Water Resources
within 30 days after the completion or abandonment of the well.

<p>1. WELL OWNER</p> <p>Name <u>C. E. DILTY</u></p> <p>Address <u>W. N. D. 11</u></p> <p>Owner's Permit No. _____</p>	<p>7. WATER LEVEL</p> <p>Static water level <u>22</u> feet below land surface.</p> <p>Flowing? <input type="checkbox"/> Yes <input type="checkbox"/> No G.P.M. flow _____</p> <p>Artesian closed-in pressure _____ p.s.i.</p> <p>Controlled by: <input type="checkbox"/> Valve <input checked="" type="checkbox"/> Cap <input type="checkbox"/> Plug</p> <p>Temperature _____ °F. Quality _____</p>																																		
<p>2. NATURE OF WORK</p> <p><input checked="" type="checkbox"/> New well <input type="checkbox"/> Deepened <input type="checkbox"/> Replacement</p> <p><input type="checkbox"/> Abandoned (describe method of abandoning) _____</p>	<p>8. WELL TEST DATA</p> <p><input type="checkbox"/> Pump <input type="checkbox"/> Bailer <input type="checkbox"/> Air <input type="checkbox"/> Other _____</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Discharge G.P.M.</th> <th>Pumping Level</th> <th>Hours Pumped</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	Discharge G.P.M.	Pumping Level	Hours Pumped																															
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<p>3. PROPOSED USE</p> <p><input checked="" type="checkbox"/> Domestic <input type="checkbox"/> Irrigation <input type="checkbox"/> Test <input type="checkbox"/> Municipal</p> <p><input type="checkbox"/> Industrial <input checked="" type="checkbox"/> Stock <input type="checkbox"/> Waste Disposal or Injection</p> <p><input type="checkbox"/> Other _____ (specify type)</p>	<p>9. LITHOLOGIC LOG</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th rowspan="2">Hole Diam.</th> <th colspan="2">Depth</th> <th rowspan="2">Material</th> <th colspan="2">Water</th> </tr> <tr> <th>From</th> <th>To</th> <th>Yes</th> <th>No</th> </tr> </thead> <tbody> <tr> <td>4</td> <td>0</td> <td>10</td> <td>Top Soil</td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td>10</td> <td>15</td> <td>CLAY 1742</td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td>15</td> <td>40</td> <td>CLAY 1742</td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td>30</td> <td>130</td> <td>NO RETURN</td> <td> </td> <td> </td> </tr> </tbody> </table>	Hole Diam.	Depth		Material	Water		From	To	Yes	No	4	0	10	Top Soil				10	15	CLAY 1742				15	40	CLAY 1742				30	130	NO RETURN		
Hole Diam.	Depth		Material	Water																															
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	10	15	CLAY 1742																																
	15	40	CLAY 1742																																
	30	130	NO RETURN																																
<p>4. METHOD DRILLED</p> <p><input checked="" type="checkbox"/> Rotary <input checked="" type="checkbox"/> Air <input type="checkbox"/> Hydraulic <input type="checkbox"/> Reverse rotary</p> <p><input type="checkbox"/> Cable <input type="checkbox"/> Dug <input type="checkbox"/> Other _____</p>	<p>10.</p> <p>Work started <u>6-3</u> finished <u>6-6</u></p>																																		
<p>5. WELL CONSTRUCTION</p> <p>Casing schedule: <input checked="" type="checkbox"/> Steel <input type="checkbox"/> Concrete <input type="checkbox"/> Other _____</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Thickness</th> <th>Diameter</th> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td><u>2.50</u> inches</td> <td><u>6</u> inches</td> <td><u>1</u> feet</td> <td><u>15</u> feet</td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table> <p>Was casing drive shoe used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Was a packer or seal used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Perforated? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>How perforated? <input type="checkbox"/> Factory <input type="checkbox"/> Knife <input type="checkbox"/> Torch</p> <p>Size of perforation _____ inches by _____ inches</p> <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Number</th> <th>From</th> <th>To</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table> <p>Well screen installed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Manufacturer's name _____</p> <p>Type _____ Model No. _____</p> <p>Diameter _____ Slot size _____ Set from _____ feet to _____ feet</p> <p>Diameter _____ Slot size _____ Set from _____ feet to _____ feet</p> <p>Gravel packed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No <input type="checkbox"/> Size of gravel _____</p> <p>Placed from _____ feet to _____ feet</p> <p>Surface seal depth <u>15</u> Material used in seal: <input type="checkbox"/> Cement grout <input checked="" type="checkbox"/> Well cuttings</p> <p><input type="checkbox"/> Pudding clay</p> <p>Sealing procedure used: <input type="checkbox"/> Slurry pit <input type="checkbox"/> Temp. surface casing <input checked="" type="checkbox"/> Overbore to seal depth</p> <p>Method of joining casing: <input type="checkbox"/> Threaded <input type="checkbox"/> Welded <input type="checkbox"/> Solvent Weld</p> <p><input type="checkbox"/> Cemented between strata</p> <p>Describe access port _____</p>	Thickness	Diameter	From	To	<u>2.50</u> inches	<u>6</u> inches	<u>1</u> feet	<u>15</u> feet													Number	From	To										<p>11. DRILLERS CERTIFICATION</p> <p>I/We certify that all minimum well construction standards were complied with at the time the rig was removed.</p> <p>Firm Name <u>C. E. DILTY</u> Firm No. <u>26</u></p> <p>Address <u>W. N. D. 11</u> Date <u>6-6-74</u></p> <p>Signed by (Firm Official) <u>J. M. ESTEY</u></p> <p>and <u>J. M. ESTEY</u></p> <p>(Operator)</p>		
Thickness	Diameter	From	To																																
<u>2.50</u> inches	<u>6</u> inches	<u>1</u> feet	<u>15</u> feet																																
Number	From	To																																	
<p>6. LOCATION OF WELL</p> <p>Sketch map location must agree with written location. 36</p> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="text-align: center;">N</td> <td style="width: 20px;"></td> <td style="text-align: center;">E</td> </tr> <tr> <td style="text-align: center;">W</td> <td style="text-align: center;">36</td> <td style="text-align: center;">E</td> </tr> <tr> <td style="text-align: center;">S</td> <td style="width: 20px;"></td> <td style="text-align: center;">E</td> </tr> </table> <p>Subdivision Name _____</p> <p>Lot No. _____ Block No. _____</p> <p>County <u>Gooding</u></p> <p><u>SE 1/4 SW 1/4 Sec. 36 T. 8 N. R. 14 E.W.</u></p>	N		E	W	36	E	S		E	<p>USE ADDITIONAL SHEETS IF NECESSARY - FORWARD THE WHITE COPY TO THE DEPARTMENT</p>																									
N		E																																	
W	36	E																																	
S		E																																	

Rev. July 17, 1967

Well Log Form 1
222

WELL LOG AND REPORT TO THE STATE RECLAMATION ENGINEER OF IDAHO

SUBMIT WITHIN 30 DAYS AFTER COMPLETION OF WELL: SEE IDAHO STATUTES 42-238

Permit No. 27900 Well No. _____ County Gooding

Owner Frank Madalena

Address Wendell, Idaho

Driller C. E. Eaton & Sons

Address Wendell, Idaho

Well location SE 1/4 SE 1/4 Sec. 31, T. 8 N/S, R. 15E/W

Size of drilled hole 12"

Total depth of well 9'

Locate well in section

NW 1/4	NE 1/4
Sec.	
SW 1/4	SE 1/4

Give depth to standing water from the ground _____ Water temp _____ °Fahr.

Test delivery was 1500 g.p.m. or _____ c.f.s. Drawdown was _____ feet. Pump? Ball? _____

Size of pump and motor used to make test 10" turbine

Length of time of test 30 min. hours _____ minutes _____

If flowing well, give flow _____ c.f.s. or _____ g.p.m. and of shut off pressure _____

If flowing well, described control works _____

(TYPE AND SIZE OF VALVE, ETC.)

Water will be used for irrigation Weight of casing per lineal foot _____

Thickness of casing _____ Casing material steel

(STEEL, CONCRETE, WOOD, ETC.)

Diameter, length and location of casing 70' x 12" from surface to 70'

(CASING 12" IN DIAMETER OR LESS, GIVE INSIDE DIAMETER; CASING OVER 12" IN DIAMETER, GIVE OUTSIDE DIAMETER)

CASING RECORD

Diam. Casing	From Feet	To Feet	Length	Remarks—seals, grouting, etc.

Number and size of perforations _____ located _____ feet to _____ feet from ground

Date of commencement of well _____ Date of completion of well October of 1961

SESE S. 31 8 S 15E

USGS

Entered in Drillers Book

WELL LOG AND REPORT TO THE STATE RECLAMATION ENGINEER OF IDAHO

RECEIVED

Log No. 1A42-1057

Rec. Department of Reclamation

Well No. _____

Permit No. 8 5 5 5 4

(DO NOT FILL IN)

Owner Ernest Weech (C. E. Weech) Address Wendell, Idaho

Driller C. B. Eaton & Sons Address Wendell, Idaho Lic. No. 28

Location of Well: 1/4 Sec. 31, T. N/S, R. 15 E/W 15 County, _____
and _____ feet N/S, and _____ feet E/W from _____ Corner of _____ 1/4 Sec. 6

Size of Drilled Hole 16 in. Total depth of Well 110 ft.

Give depth of standing water from surface 8 1/2 ft. Water Temp. _____ °Fahrenheit

On pumping test delivery was 900 g.p.m. or _____ c.f.s. Drawdown was 110 feet.

Size of pump and motor used to make the test 20 h.p. turbin pump

Length of time pumped during check was _____ hr., _____ minutes.

If flowing well, give flow in c.f.s. _____ or g.p.m. _____ and shut in pressure _____

If flowing well, describe control works _____
(TYPE AND SIZE OF VALVE, ETC.)

Water will be used for irrigation Weight of casing per linear foot _____

Thickness of casing 12 g. Casing material _____
E.G., PIPE, CONCRETE, WOOD.

Diameter, length and location of casing 6 ft. surface pipe
(CASING 12" IN DIAMETER AND UNDER GIVE INSIDE DIAMETER;
CASING OVER 12" IN DIAMETER GIVE OUTSIDE DIAMETER.)

Number and size of perforations _____ located _____ feet to _____ feet
from surface of ground.

Other perforations _____

Date of commencement of well _____ Date of completion of well September 1, 1957

Type of well rig Spudder

CASING RECORD

DIAM. CASING	FROM FEET	TO FEET	LENGTH	"REMARKS" -- SEALS, GROUTING, ETC.
<u>5 1/2"</u>				

GENERAL INFORMATION—Pumping Test, Quality of Water, Etc.

SWSE S. 31 85 15E

STATE OF IDAHO
DEPARTMENT OF WATER RESOURCES
WELL DRILLER'S REPORT

The Law requires that this report be filed with the Director, Department of Water Resources within 30 days after the completion or abandonment of the well.

1. WELL OWNER
 Name: Bill Fleming
 Address: Wendell
 Owner's Permit No. _____

7. WATER LEVEL
 Static water level 90 feet below land surface.
 Flowing? Yes No G.P.M. flow _____
 Artesian closed-in pressure _____ p.s.i.
 Controlled by: Valve Cap Plug
 Temperature _____ of. Quality _____

2. NATURE OF WORK
 New well Deepened Replacement
 Abandoned (describe method of abandoning) _____

8. WELL TEST DATA

Discharge G.P.M.	Pumping Level	Hours Pumped

3. PROPOSED USE
 Domestic Irrigation Test Municipal
 Industrial Stock Waste Disposal or Injection
 Other _____ (specify type)

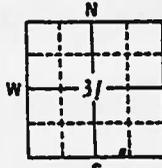
9. LITHOLOGIC LOG

Hole Diam.	Depth		Material	Water	
	From	To		Yes	No
8	0	5	top soil		✓
8	5	19	gray lava		✓
4	19	60	" "		
4	60	75	gray lava		✓
7.5	75	305	gray lava		✓

4. METHOD DRILLED
 Rotary Air Hydraulic Reverse rotary
 Cable Dug Other _____

5. WELL CONSTRUCTION
 Casing schedule: Steel Concrete Other _____
 Thickness _____ Diameter _____ From _____ To _____
260 inches 10 inches + 1 feet 19 feet
 _____ inches _____ inches _____ feet _____ feet
 _____ inches _____ inches _____ feet _____ feet
 _____ inches _____ inches _____ feet _____ feet
 Was casing drive shoes used? Yes No
 Was a packer or seal used? Yes No
 Perforated? Yes No
 How perforated? Factory Knife Torch
 Size of perforation _____ inches by _____ inches
 _____ Number _____ From _____ To _____
 _____ perforations _____ feet _____ feet
 _____ perforations _____ feet _____ feet
 _____ perforations _____ feet _____ feet
 Well screen installed? Yes No
 Manufacturer's name _____
 Type _____ Model No. _____
 Diameter _____ Slot size _____ Set from _____ feet to _____ feet
 Diameter _____ Slot size _____ Set from _____ feet to _____ feet
 Gravel packed? Yes No Size of gravel _____
 Placed from _____ feet to _____ feet
 Surface seal depth 19 Material used in seal: Cement grout
 Puddling clay Well cuttings
 Sealing procedure used: Slurry pit Temp. surface casing
 Overbore to seal depth
 Method of joining casing: Threaded Welded Solvent
 Weld
 Cemented between strata
 Describe access port _____

RECEIVED
 JUL 2 1981
 Department of Water Resources
 RECEIVED
 JUN 26 1981
 Dec. _____

6. LOCATION OF WELL
 Sketch map location must agree with written location.

 Subdivision Name _____
 Lot No. _____ Block No. _____
 County Blaine
S W 1/4 Sec. 31, T. 8 N, R. 16 E.

10. Work started April 13 finished April 24-81
11. DRILLERS CERTIFICATION.
 I/We certify that all minimum well construction standards were complied with at the time the rig was removed.
 Firm Name C B Eaton & Son Firm No. 26
 Address Wendell 102 Date 4-23-81
 Signed by (Firm Official) James Eaton
 and
 (Operator) Wendell

**WELL LOG AND REPORT TO THE
STATE RECLAMATION ENGINEER OF IDAHO**

Log No. _____

Rec. June 18 1952

Well No. _____

Permit No. P-24112

DO NOT FILL IN

Owner William Grissom Driller Zaton & Sons

Address Wendell, Idaho Address Wendell, Idaho Lic. No. 2

Location of Well: N.W. 1/4, S.E. 1/4 Sec. 36, T. 8 N, R. 14 E, GARDING County.

and _____ feet N/S, and _____ feet E/W from _____ corner of _____ 1/4 _____ 1/4 Sec. _____

Water will be used for Irrigation & domestic Total depth of well 98 feet

Size of drilled hole 12" Weight of casing per linear foot _____

Thickness of casing _____ Casing Material _____
e.g. pipe, concrete, wood.

Diameter, length and location of casing _____
(Casing 12" in diameter and under give inside diameter; casing over 12" in diameter give outside diameter.)

Number and size of perforations _____ located _____ feet to _____ feet

from surface of ground.

Other Perforations: _____

If flowing well, give flow in c.f.s. _____ or g.p.m. 450 and shut in pressure _____

If nonflowing well, give depth of standing water from surface 72 feet

If flowing well, describe control works _____

On pumping test delivery was 450 g.p.m. or _____ c.f.s. Drawdown was none feet
(Type and size of valve, etc.)

Length of time pumped during check was week hr. _____ min. Water temp. 60 °Fahrenheit.

Date of commencement of well May, 1952 Date of Completion of well May, 1952

Type of well rig SPUDING

CASING RECORD

Diam. Casing	From Feet	To Feet	Length	Remarks—Seals, Grouting, Etc.
12			8 ft	Through top soil cement

GENERAL INFORMATION—Pumping Test, Quality of Water, Etc.

W.A.E. 5.36 8.5 14E

Permit 24112

52

APPENDIX D

Slug Test Data and Computations

Tested 7-16-91

Clear Lakes

Hydraulic Conductivity - MW 3D

$$L = 212 - 185 = 27' \quad (\text{bottom of screen } \& \text{ avg. water level})$$

$$H = 27'$$

$$D = 270' - 185' = 85' \quad (\text{from possible basalt lens or sandstone up } \& \text{ water level})$$

$$r_w = 0.33'$$

$$r_c = 0.17'$$

$$1) \ln \frac{H}{r_w} = \ln \frac{27}{0.33} = 4.40$$

$$2) \frac{L}{r_w} = 81.82$$

$$3) \boxed{A = 3.8} \quad \boxed{B = 0.7}$$

$$4) \ln \left(\frac{D-H}{r_w} \right) = \ln \left(\frac{85-27}{0.33} \right) = \boxed{5.17}$$

$$5) \text{ let } t = 100 \text{ sec} \quad y_0 = 10.5' \quad y_t = 6.0'$$

$$\left(\frac{1}{t} \right) \ln \frac{y_0}{y_t} = \frac{1}{100} \ln \frac{10.5}{6.0} = \boxed{0.006}$$

$$6) \ln \frac{r_c}{r_w} = \left[\frac{1.1}{\ln \left(\frac{H}{r_w} \right)} + \frac{A + B \ln \left(\frac{D-H}{r_w} \right)}{\frac{L}{r_w}} \right]^{-1}$$

$$\ln \frac{r_c}{r_w} = \left(\frac{1.1}{4.40} + \frac{3.8 + 0.7(5.17)}{81.82} \right)^{-1} = \boxed{2.94}$$

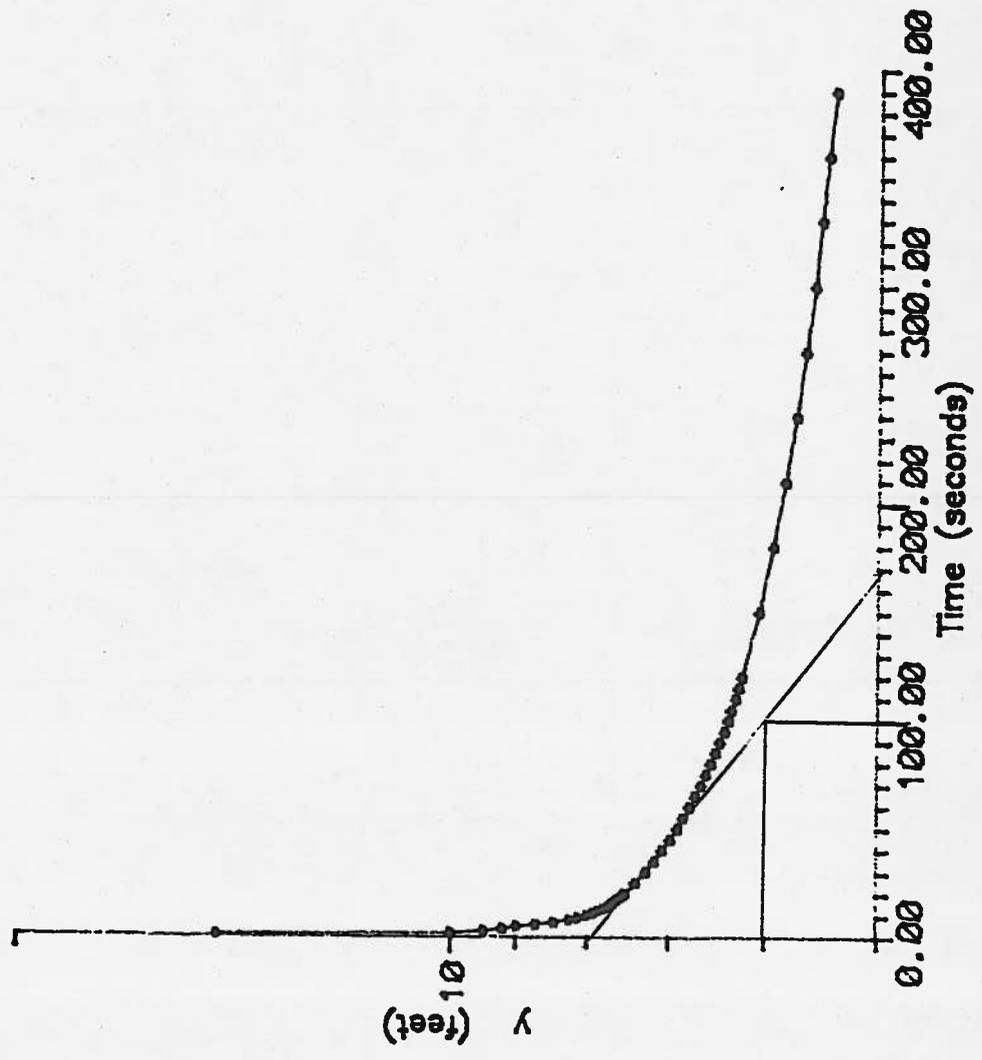
$$7) K = \frac{r_c^2 \ln \frac{r_c}{r_w}}{2L} \cdot \frac{1}{t} \ln \frac{y_0}{y_t}$$

$$K = \frac{(0.17)^2 \cdot 2.94}{2(27)} \cdot 0.006$$

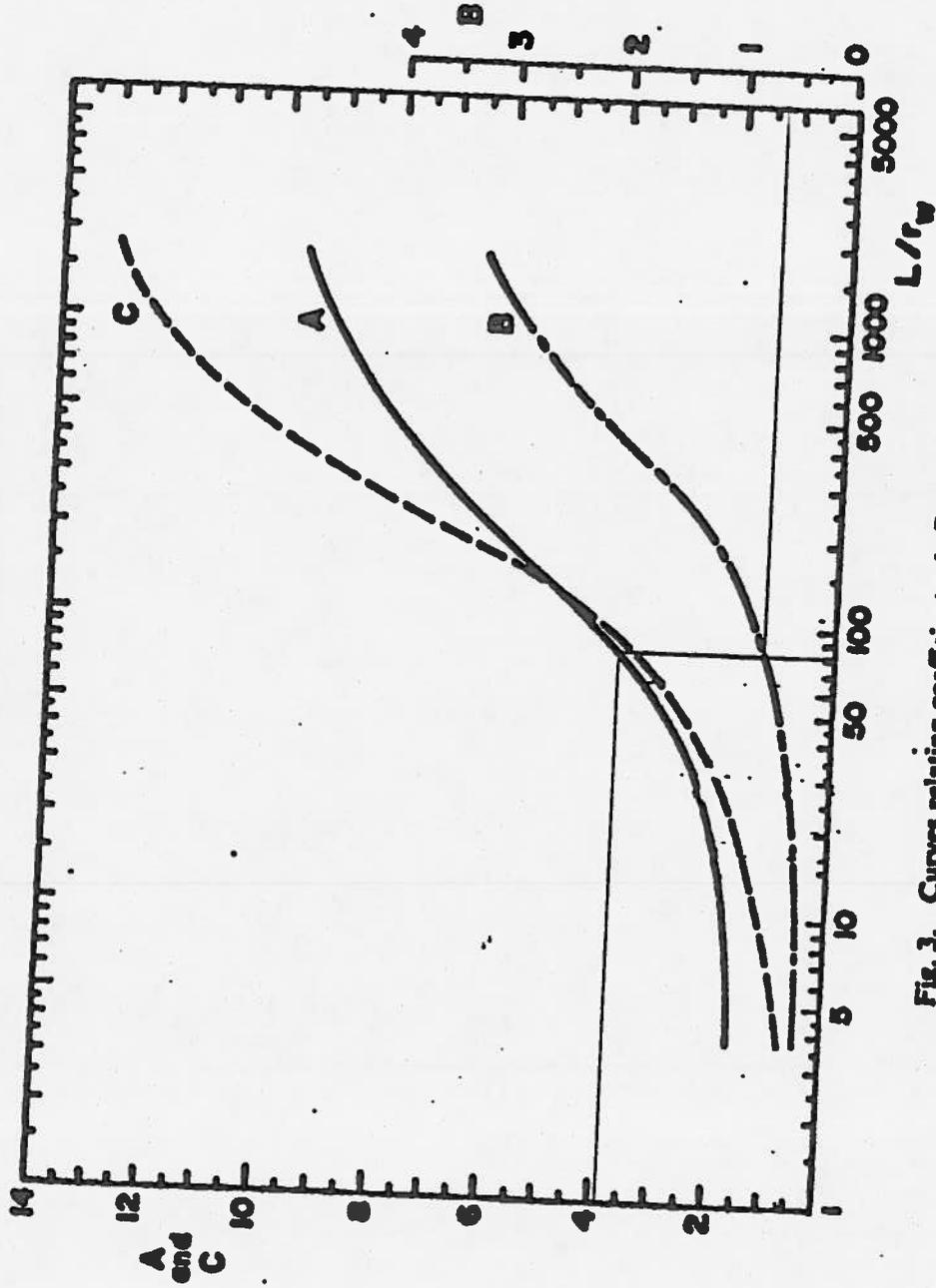
$$K = 9.4 \times 10^{-6} \frac{\text{ft}}{\text{sec}} = 6.07 \frac{\text{gal}}{\text{ft} \cdot \text{day}}$$

$$\times 1.34 = \text{ft/day} \quad \boxed{.81 \text{ ft/day}}$$

Water Level Recovery Vs. Time For Slug Test On
Monitoring Well MW-3D



BOUWER AND RICE: GROUNDWATER HYDRAULICS



Clear Lakes
Well MW-3D

Fig. 3. Curves relating coefficients A, B, and C to L/r_w .

Tested 7-16-91

Clear Lakes

Hydraulic Conductivity: MW-2

$L = 249 - 230 = 19'$ (screened interval submerged in H₂O)

$H = 249 - 195 = 54'$ (bottom of screen to avg. H₂O level)

$D = 270 - 195 = 75'$ (sandstone/basalt layer up to H₂O level)

$r_w = 0.33'$

$r_c = 0.17'$

1) $\ln \frac{H}{r_w} = \ln \frac{54}{0.33} = 5.10$

2) $\frac{L}{r_w} = \frac{19}{0.33} = 57.58$

3) $A = 3.3$ $B = 0.5$

4) $\ln \left(\frac{D-H}{r_w} \right) = \ln \frac{75-54}{0.33} = 4.15$

5) let $t = 50 \text{ sec}$ $y_0 = 4.2'$ $y_t = 0.55'$
 $\frac{1}{t} \ln \frac{y_0}{y_t} = \frac{1}{50} \ln \frac{4.2}{0.55} = 0.041$

6) $\ln \frac{r_e}{r_w} = \left[\frac{1.1}{\ln \left(\frac{H}{r_w} \right)} + \frac{A + B \ln \left(\frac{D-H}{r_w} \right)}{\frac{L}{r_w}} \right]^{-1}$

$\ln \frac{r_e}{r_w} = \left(\frac{1.1}{5.10} + \frac{3.3 + 0.5(4.15)}{57.58} \right)^{-1} = 0.16$

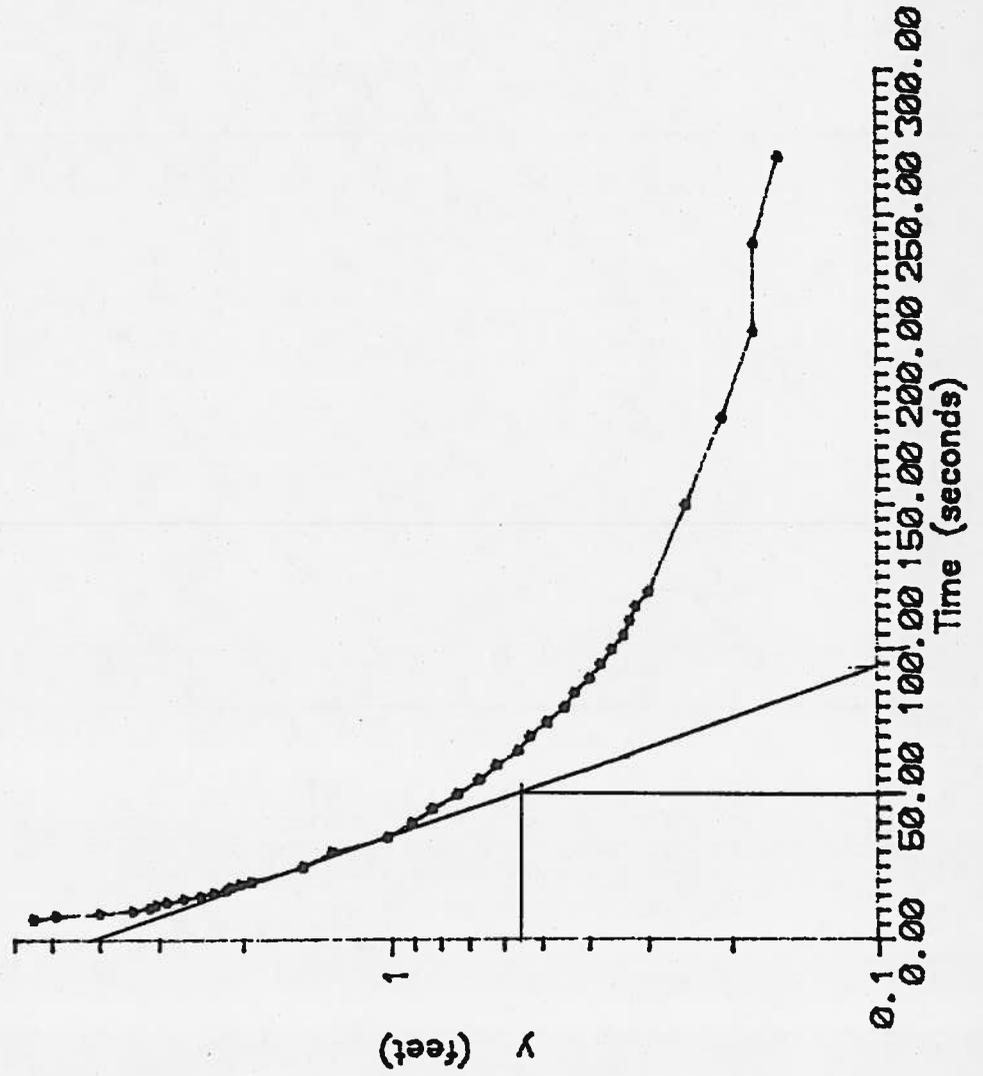
7) $K = \frac{r_c^2 \ln \frac{r_e}{r_w}}{2L} \cdot \frac{1}{t} \ln \frac{y_0}{y_t}$

$K = \frac{(0.17)^2 (0.16)}{2(19)} \cdot 0.041$

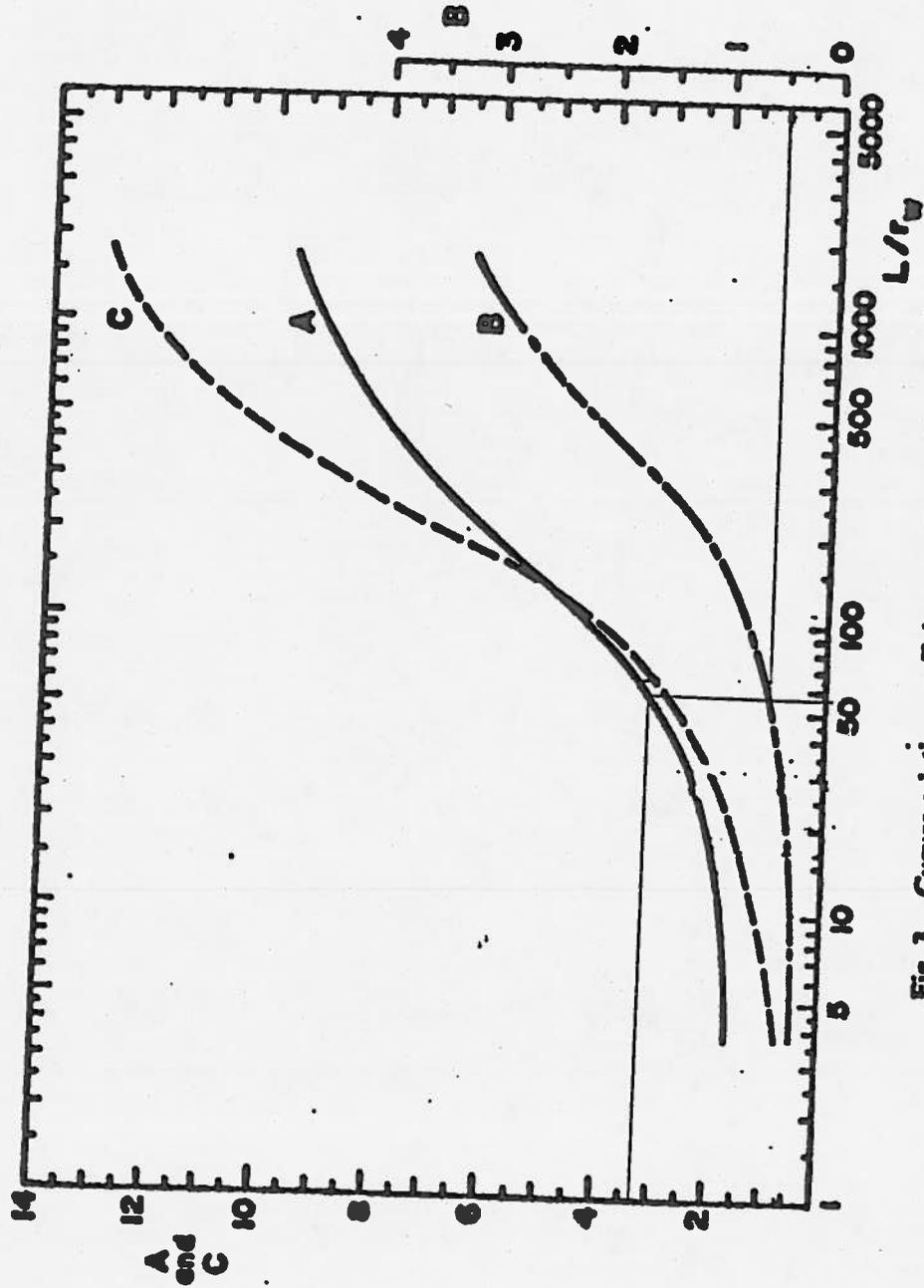
$K = 4.99 \times 10^{-6} \frac{\text{ft}}{\text{sec}} = 3.22 \frac{\text{gal/day}}{\text{ft}^2}$

43 ft/day

Water Level Recovery Vs. Time For Slug Test On
Monitoring Well MW-2



BOUWER AND RICE: GROUNDWATER HYDRAULICS



Clear Lakes
Well MWZ

Fig. 3. Curves relating coefficients A, B, and C to L/r_w .

APPENDIX E

Pump Tests and Modeling Data

A computer model was used to estimate groundwater fluctuations due to the construction of the proposed road cut. Input data for the model included measured and assumed bedrock hydraulic conductivities, groundwater gradients, proposed road cut geometry, and various boundary conditions.

Data was evaluated using the U.S.G.S. MODFLOW groundwater flow model (McDonald and Harbaugh, 1988). MODFLOW is a three-dimensional model which allows simulation of a heterogenous aquifer with boundary conditions and steady or transient state conditions.

Executing MODFLOW involves dividing the area of interest into blocks by superimposing a rectangular grid over the modeled area. Each block is then assigned aquifer parameters. MODFLOW then formulates an equation for groundwater flow based on Darcy's law for fluid movement in a porous medium.

The proposed road cut was modeled using a single layer 40 by 18 node grid, centered over the cut face. The southern boundary of the grid was aligned along the top of the canyon rim. The grid was placed in this manner to allow simulation of spring and road cut drainage; the grid extends north, east, and west to the assumed boundary conditions for the modeled area. The southern boundary was modeled with drainage nodes to simulate water lost through spring flow. The elevations of the drain nodes were determined based on known groundwater elevations and gradient of the shallow water-bearing unit. The northern edge of the modeled area is represented with a constant-head boundary with head values corresponding to known groundwater elevations. Execution of the model under these conditions developed an estimate of total spring discharge and allowed calibration of the model to observed conditions.

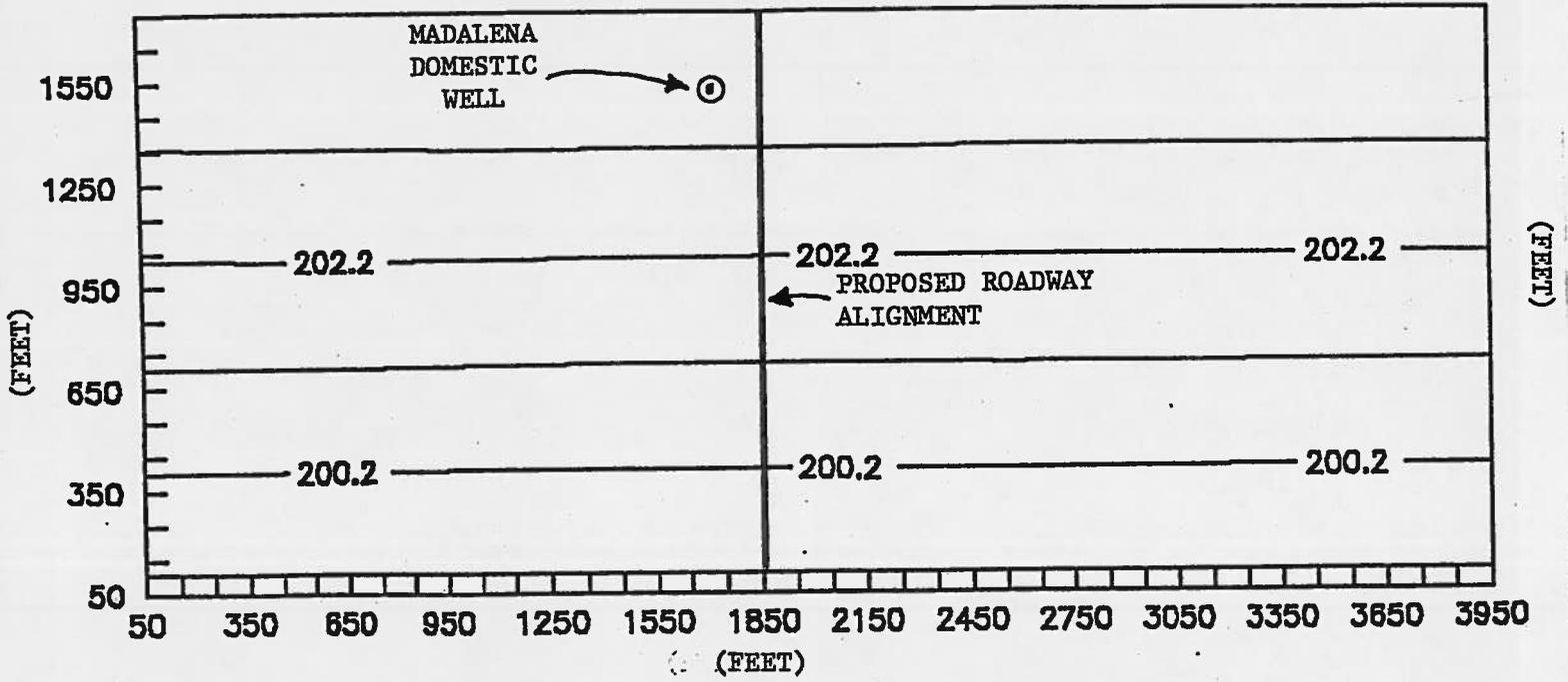
A second model was developed that simulated the proposed road cut by using drain nodes along the southern boundary and cut area. The nodes were placed along saturated portions of the cut at elevations approximating the final road grade. By using drain nodes to simulate the cut, a water budget can be calculated by the model which provides an estimated groundwater flow rate.

Estimates of groundwater flow from the proposed road cut were determined using the following methodology:

- o Constant-head boundaries were established on the north boundary of the grid. Drain nodes were placed along the southern boundary to simulate spring discharge;
- o Nodes were assigned hydraulic conductivity values based on aquifer pump test data and values for fractured bedrock obtained from Freeze and Cherry (1979);

- o The initial model was run until steady state conditions were achieved to generate a flow field across the domain corresponding to pre-construction conditions. This allows verification of the assumed boundary conditions and aquifer parameters;
- o A second model simulating the road cut was also run until steady state conditions were obtained. The difference in water volume collected in the drain nodes from the pre-construction model with the second model following road construction represents the volume of water flowing from the completed road cut.

WATER TABLE PRE-GRADE



WATER TABLE WITH GRADE

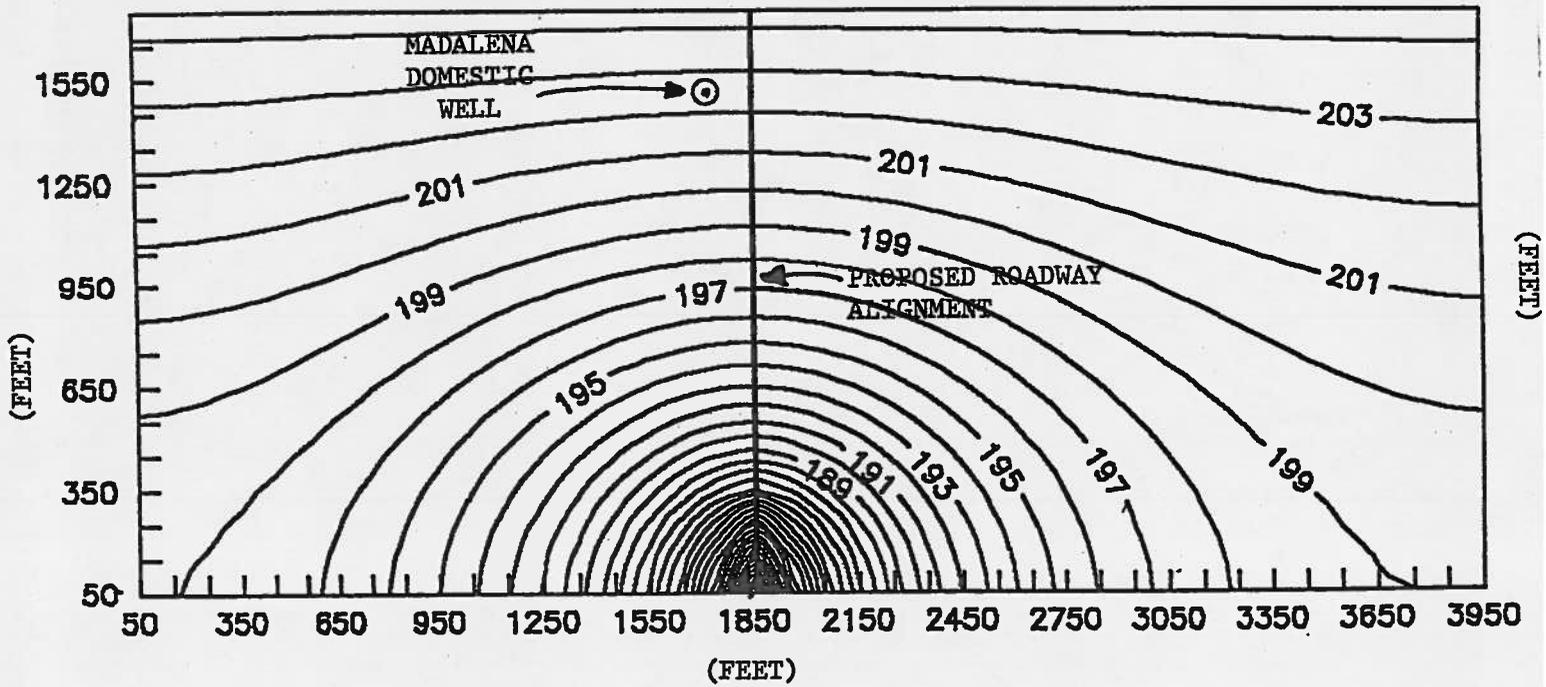
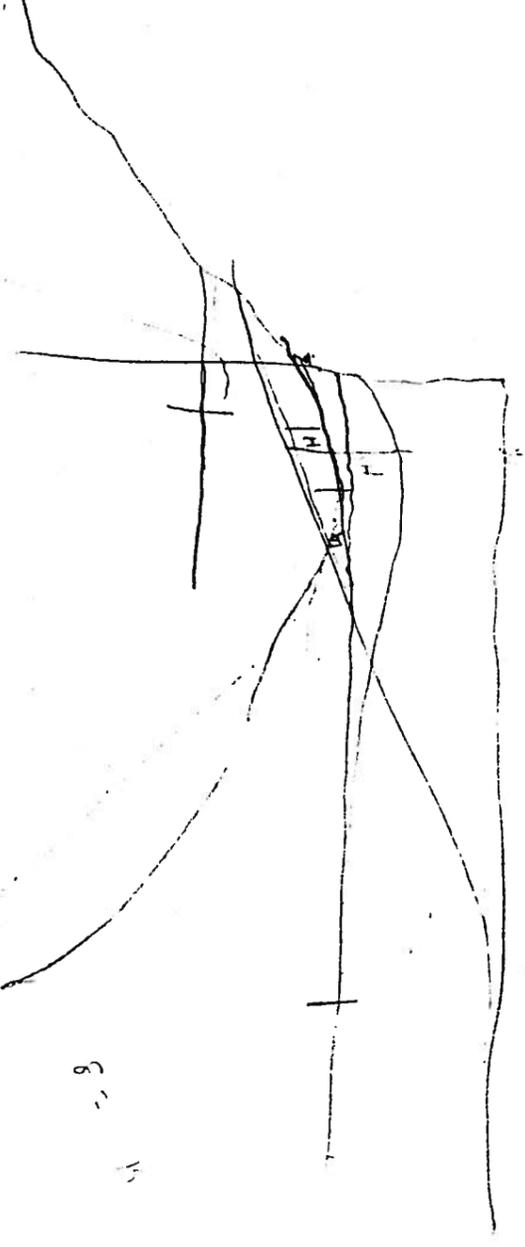


FIGURE 11

ESTIMATED GROUNDWATER LEVEL CHANGES
INDUCED BY THE PROPOSED ROADCUT

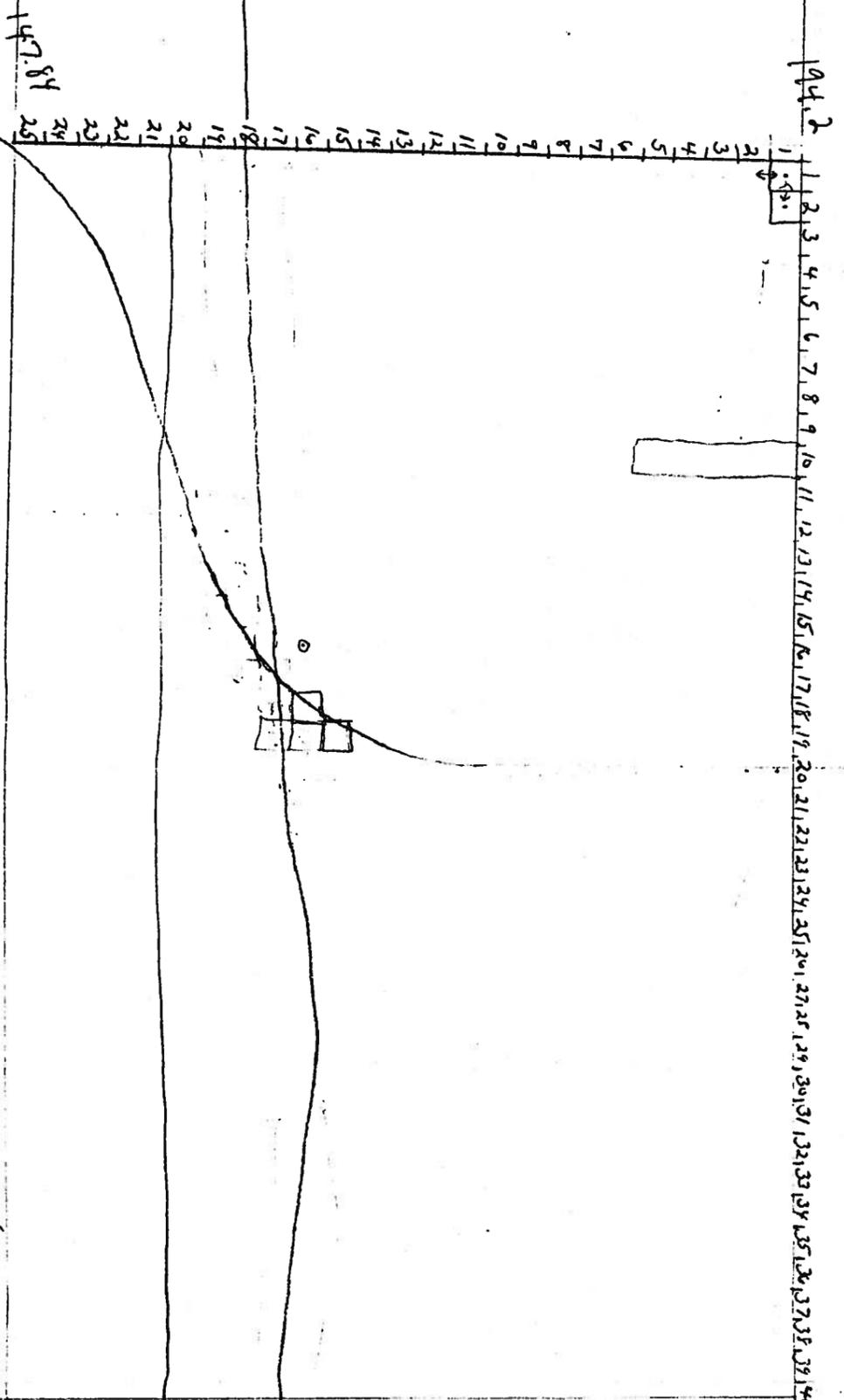
DRAINS OUT = 32,622,000 Ft³/day
 KORN OUT 42,510,000



DRAIN HOLES

L	R	ELEV
11	15	162
18	16	159
17	17	150
16	18	153
15	18	150
14	19	177
13	20	145

SPRING HOLES = 202.6
 Row 18



06/08 12:38:28 N1.95

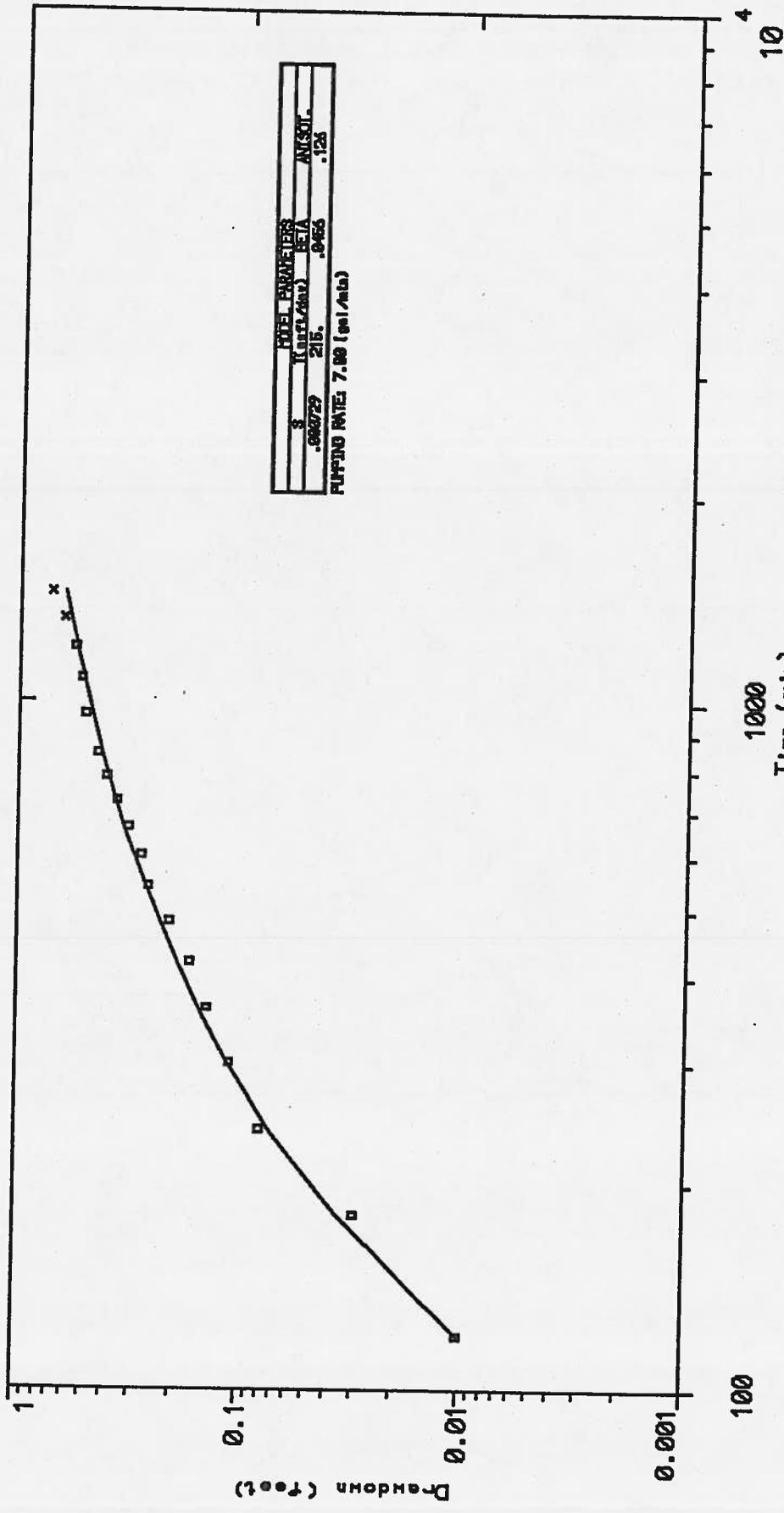
L = .0036
 46 columns
 25 Rows

DX = DY = 160'
 BASE = 3/50

-DRAIN	ELEV.	ROW
1	164	18
2	171	17
3	178	15
4	185	15
5	192	14
6	199	13

DRAIN HOLES REVERTED TO SPRING LINE = 2

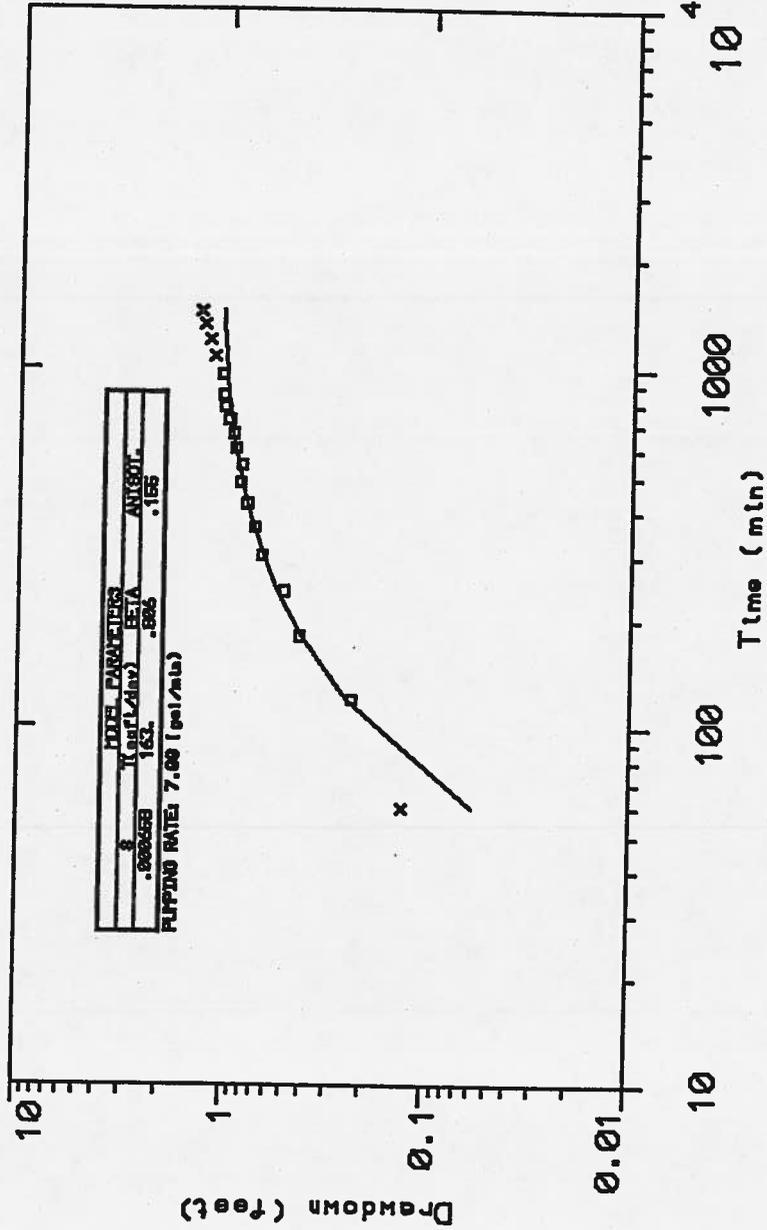
HEAD = 147.84



MODEL PARAMETERS	
S	AK301.
K (cm ² /day)	215.
BETA	0.465
AK301.	0.128

PUMPING RATE: 7.00 (gal/min)

for:	SHARP AND SMITH	CLEAR LAKES GRADE
by:	Chen-Northern	BUHL, IDAHO
Aquifer: FRACTURED BASALT		GOODING COUNTY
Thickness: 125.		
Screen: Base: 100. Top: 80.0 feet		
Distance: 560. feet Pumping well: MW-1S		
		Date: 10 SEPT 91
		Well No.: MW-4S



MODEL PARAMETERS	
W (in/L/min)	ANTIBOT.
0.00058	0.155
132	0.895
PUMPING RATE: 7.00 (gal/min)	

for: SHARP AND SMITH	CLEAR LAKES GRADE
by: Chen-Northern	BUHL, IDAHO
Aquifer: FRACTURED BASALT	GOODING COUNTY
Thickness: 125.	Depth: 118. feet
Screen: Base: 100.	Top: 80.0 feet
Distances: 280. feet	Pumping Well: M4-18
Date: 10 SEPT 91	Well No.: B-1

AQUIFER TEST DATA

WELL OBSERVED MW1-5
 (Data Reported on This Form)
 WELL TESTED MW1-5
 TEST DATE 9/10/91

Project Clear Lakes Grade Personnel D May

State Idaho County _____
 WELL DESCRIPTION
 Location: T _____ R _____ Sec. _____ Tract _____
 Borehole Diam. (in) _____ Well Diam. (in) _____ Well Depth (ft) 105 Perforated Zone(s) (ft) 80'-100
 Desc. of HP _____ Stick-up (ft) _____ SWL below HP (ft) _____ SWL below GS (ft) 73.35

Aquifer Name _____ Aquifer Description _____
 (Lithology, Thickness, Depth to Top)
 TEST DESCRIPTION:

- Test Type: (Circle One)
- 1. Pumping Well Drawdown
 - 2. Observation Well Drawdown
 - 3. Pumping Well Recovery
 - 4. Observation Well Recovery
 - 5. Bailor Recovery
 - 6. Slug Injection or Removal
 - 7. Hvorslev Test
 - 8. Other (Specify) _____

Distance of Observation Well from Pumping Well (ft) _____ Pump hp. & type _____ Pump Depth (ft) _____

Water Quality Sample Taken? yes no Specific Conductance ($\mu\text{mhos/cm}$ @ 25°C) _____ Temp (°C) _____ Time _____

Avg. Discharge (gpm) _____ Test Duration (min) _____ Max WL Change (ft) _____ Transmissivity (gpd/ft) _____

Storativity _____ Hydraulic Conductivity (gpd/ft²) _____ Specific Capacity (gpm/ft of drawdown) _____

REMARKS _____

Date & hour	Time	Head (ft)	SWL	Q	SC	PH		
9/10/91	11:47	26.25		5 gal in 25 sec				
	off at 1200	8.95						
	1230	26.82		5 gal in 32.0 sec				
	1330	19.17			553.5	7.11		
	1430	16.21		5 gal in 36 sec				
	1530	14.40						
	1630	12.62		5 gal in 39 sec				
	1730	11.37			552.5	7.45		
	1830	10.16		5 gal in 41.35 sec				
	1930	9.02						
	2030	8.27		5 gal in 42.30 sec				
	2130	7.52			545.5	7.40		
	2230	6.55		5 gal in 42.77 sec				
	2300	5.80						
	2330	6.75		5 gal in 43.9 sec				
9/11/91	0030	6.45						
	0130	5.53		5 gal in 44.65 sec				
	0230	5.98			554.01	7.46		
	0330	6.84		5 gal in 44.55 sec				
	0430	5.90						
	0530	5.20		5 gal in 45.59 sec				
	0630	6.80			548.12	7.49		

closed down valve to Kapier and near 16'

adjust valve
 adjust valve @ 0300
 adjust @ 0547

WELL OBSERVED MW 4-S
 (Data Reported on This Form)
 WELL TESTED MW 1-S
 TEST DATE 9/10/91

Project Clean Lakes Grade Personnel D May

State Idaho County _____ WELL DESCRIPTION _____
 Location: T _____ R _____ Sec. _____ Tract _____

Borehole Diam. (in) 8 Well Diam. (in) 4 Well Depth (ft) 110 Perforated Zone(s) (ft) 84.6 - 104.3

Desc. of MP Toy-OK PVC Stick-up (ft) _____ SWL below MP (ft) 70.75 SWL below GS (ft) _____

Aquifer Name FA Aquifer Description FRAGMENTED BASALT
 (Lithology, Thickness, Depth to Top)
 TEST DESCRIPTION _____

- Test Type: (Circle One)
- 1. Pumping Well Drawdown
 - 2. Observation Well Drawdown
 - 3. Pumping Well Recovery
 - 4. Observation Well Recovery
 - 5. Bailor Recovery
 - 6. Slug Injection or Removal
 - 7. Hvorslev Test
 - 8. Other (Specify) _____

Distance of Observation Well from Pumping Well (ft) 560 Pump hp. & type 3/4 Pump Depth (ft) _____

Water Quality Sample Taken? yes no Specific Conductance ($\mu\text{mhos/cm @ } 25^\circ\text{C}$) _____ Temp ($^\circ\text{C}$) _____ Time _____

Avg. Discharge (gpm) _____ Test Duration (min) _____ Max WL Change (ft) .63 Transmissivity (gpd/ft) _____

Storativity _____ Hydraulic Conductivity (gpd/ft²) _____ Specific Capacity (gpm/ft of drawdown) _____

REMARKS _____

Date & hour	Time	SWL				
9/10/91	1330	73.78			60	0.01
	1430	73.79			120	0.03
	1530	73.81			180	0.08
	1630	73.82			240	0.11
	1730	73.89			300	0.14
	1830	73.92			360	0.17
	1930	73.86	Drifted	100 ft	420	0.21
	2030	73.90			480	0.26
	2130	73.95			540	0.28
	2230	73.97			600	0.32
	2330	74.01			660	0.36
	0030	74.05			720	0.40
	0130	74.09			780	0.44
	0230	74.13			840	0.47
	0330	74.16			900	0.50
	0430	74.19			960	0.51
	0530	74.20			1020	0.52
	0630	74.21			1080	0.54
	0730	74.23			1140	0.54
	0830	74.25			1200	0.58
	0930	74.27			1260	0.63
	1030	74.32			1320	0.69
	1130	74.38			1380	

WELL OBSERVED B7
 (Data Reported on This Form)
 WELL TESTED MW1-5
 TEST DATE 9/10/91

Project Clear Lakes Grade Personnel D. Moy

State Idaho County _____ WELL DESCRIPTION Location: T _____ R _____ Sec. _____ Tract _____

Borehole Diam. (in) _____ Well Diam. (in) 1" Well Depth (ft) 118 Perforated Zone(s) (ft) 98-118
 Desc. of MP TOP OF PVC Stick-up (ft) 7.0' SWL below MP (ft) 72.59 SWL below GS (ft) 72.43

Aquifer Name SNAKE RIVER BASALT Aquifer Description FRACTURED BASALT
 (Lithology, Thickness, Depth to Top)
 TEST DESCRIPTION

- Test Types (Circle One)
- 1. Pumping Well Drawdown
 - 2. Observation Well Drawdown
 - 3. Pumping Well Recovery
 - 4. Observation Well Recovery
 - 5. Bailor Recovery
 - 6. Slug Injection or Removal
 - 7. Hvorslev Test
 - 8. Other (Specify) _____

Distance of Observation Well from Pumping Well (ft) 280' Pump hp. & type _____ Pump Depth (ft) _____

Water Quality Sample Taken? yes no Specific Conductance ($\mu\text{mhos/cm @ } 25^\circ\text{C}$) _____ Temp ($^\circ\text{C}$) _____ Time _____

Avg. Discharge (gpm) _____ Test Duration (min) _____ Max WL Change (ft) _____ Transmissivity (gpd/ft) _____

Storativity _____ Hydraulic Conductivity (gpd/ft²) _____ Specific Capacity (gpm/ft of drawdown) _____

REMARKS

Date & hour	Time	t	SWL (ft)	S				
9/10/91	1230		72.59	"				
	1330	60	72.72	0.13				
	1430	120	72.82	0.23				
	1530	180	73.01	0.42				
	1630	240	73.10	0.51				
	1730	300	73.25	0.66				
	1830	360	73.31	0.72				
	1930	420	73.38	0.79				
	2030	480	73.44	0.85				
	2130	540	73.48	0.89				
	2230	600	73.49	0.90				
	2330	640	73.52	0.93				
9/11/91	0030	720	73.57	0.98				
	0130	780	73.62	1.03				
	0230	840	73.62	1.03				
	0330	900	73.63	1.04				
	0430	960	73.65	1.04				
	0530	1020	73.66	1.07				
	0630	1080	73.74	1.15				
	0730	1140	73.78	1.19				
	0830	1200	73.81	1.22				
	0930	1260	73.87	1.28				
	1030	1320	73.89	1.30				

C V F R

